

Serpent-OpenFOAM coupling for criticality accidents modelling

—

Definition of a benchmark for MSRs multiphysics modelling

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Serpent-OpenFOAM coupling for criticality accidents

Validation against Godiva burst experimental data

Application to the MSFR transient simulation

Definition of a benchmark for MSRs multiphysics modelling



SERPENT/OpenFOAM internal coupling in transient mode

OpenFOAM libraries dynamically linked to Serpent-2 at source code level

- Neutron transport via standard SERPENT Monte Carlo routines
- Other physics are solved with standard OpenFOAM Finite-Volumes methods
- Coupling is performed at runtime
- Code-to-code coupling & complex I/O files are avoided
- Fast and flexible mesh handling and deformation
- Preliminary validation on Godiva super prompt critical transients



Assessment and verification: Godiva super prompt-critical burst

Godiva: spherical assembly ~ 50 kg of metallic U



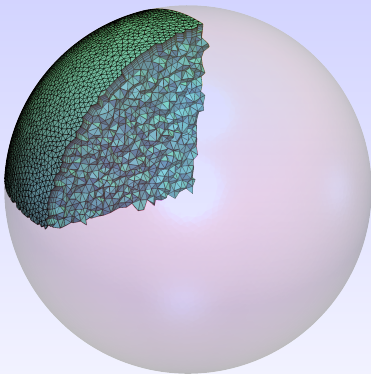
- Experimental results from LA-2029 (1960, public release 1995?)
- Effective prompt lifetime = few ns
- Rapid power excursion
- Thermal expansion feedbacks (no Doppler)
- In fast transients ($T \sim 10 \mu s$) speed of sound (few km/s) is relatively small: thermal-expansion is not in equilibrium with temperature fields

Modelling conditions “close” to MSFR super prompt-critical transients



Assessment and verification: Godiva super prompt-critical burst

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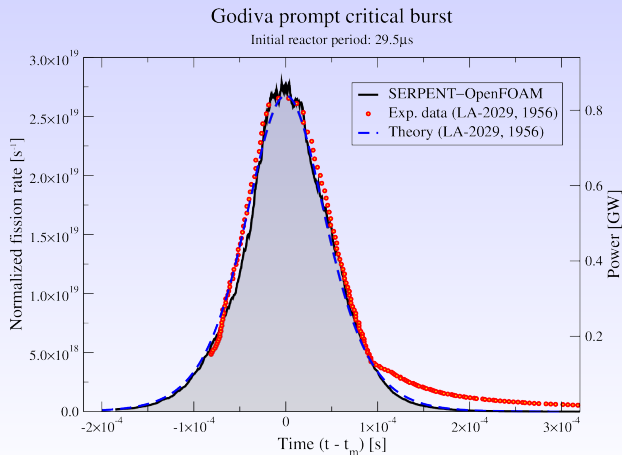
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Godiva super prompt-critical burst

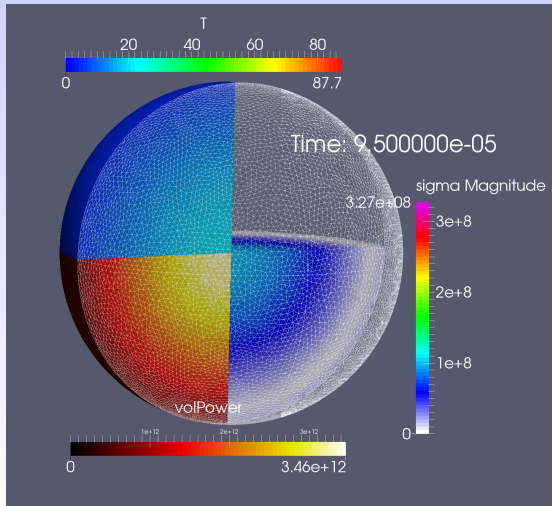
Initial reactor periods: 11.6 and 29.5 μs

Validation against Los Alamos experimental data



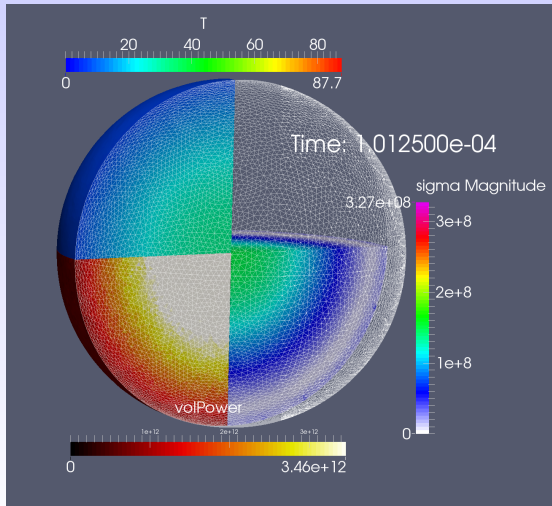
Godiva super prompt-critical burst

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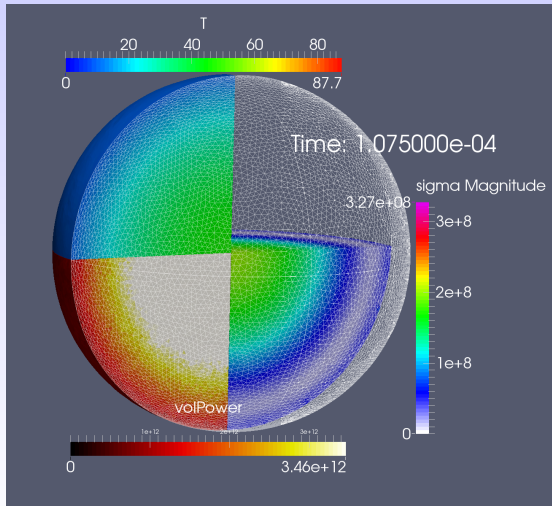
Godiva super prompt-critical burst

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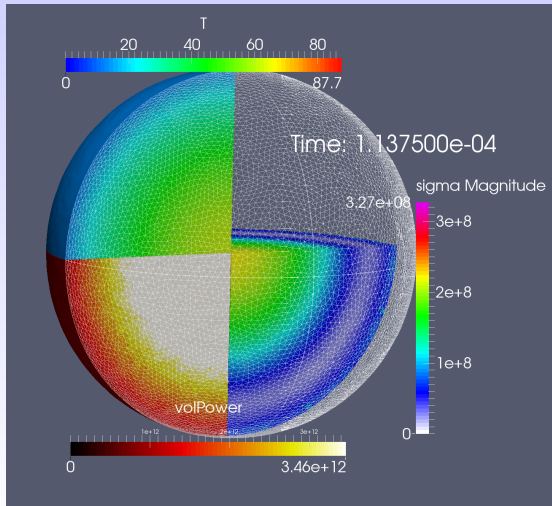
Godiva super prompt-critical burst

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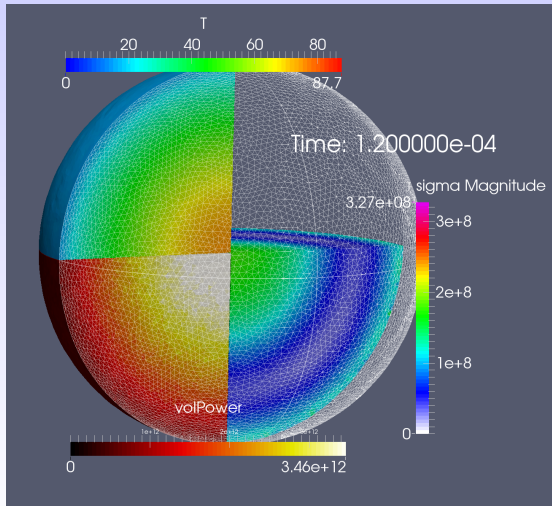
Godiva super prompt-critical burst

Initial reactor periods: 11.6 and 29.5 μs



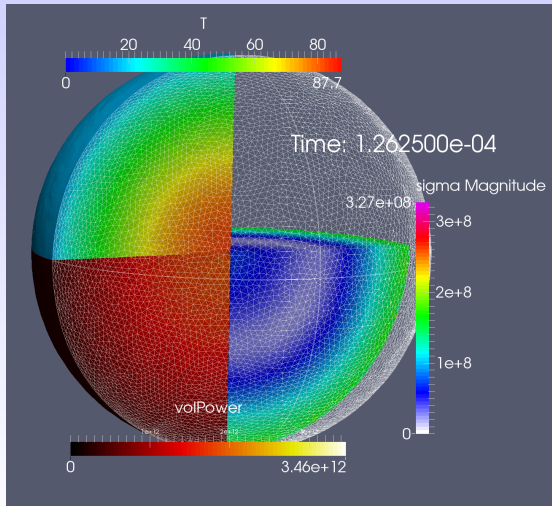
Godiva super prompt-critical burst

Initial reactor periods: 11.6 and 29.5 μs



Godiva super prompt-critical burst

Initial reactor periods: 11.6 and 29.5 μs



Serpent-OpenFOAM coupling... how does it work?

Linear elasticity

$$\rho \frac{\partial^2}{\partial t^2} = \nabla \left[\mu \nabla + \mu (\nabla)^T + \lambda \mathbf{I} \text{tr}(\nabla) \right] + \nabla \left(\frac{E}{1-2\nu} \alpha T \right) \quad (1)$$

$$\mu = \frac{E}{2(1+\nu)}; \quad \lambda = \frac{\nu E}{(1+\nu)(1-2\nu)} \quad (2)$$

Energy equation

$$\frac{\partial T}{\partial t} = \frac{k}{\rho c} \nabla^2 T + \frac{q'''_{\text{fission}}}{\rho c} \quad (3)$$



Serpent-OpenFOAM coupling... how does it work?

Score fission energy deposition

Code snippet – OpenFOAMScoreFissionEnergy.cpp

```
void OFScoreFissE(long mat, long part, ... , indexedOctree<treeDataCell>& ioc)
{
    ...
    if (mat > VALID_PTR)
    {
        if ((rea = (long)RDB[mat + MATERIAL_PTR_FISSE]) > VALID_PTR)
        {
            if ((fissE = MacroXS(rea, E, id)*flx*g*wgt) > 0.0)
            {
                point sample(x/100.0, y/100.0, z/100.0);
                sampleCellIndex = ioc.findInside(sample);
                volPowerBuffer.internalField()[sampleCellIndex] += fissE;
            }
        }
    }
}
```



Serpent-OpenFOAM coupling... how does it work?

Material density at collision points

Code snippet – OpenFOAMDensityFactor.cpp

```
double OFDensityFactor(..., volScalarField& rhok, indexedOctree<treeDataCell>&
    ioc)
{
    double f;
    Foam::label sampleCellIndex;

    ...

    point sample(x/100.0, y/100.0, z/100.0);
    sampleCellIndex = ioc.findInside(sample);

    if (sampleCellIndex != -1)
        f = rhok.internalField()[sampleCellIndex];
    else
        f = 0.0;

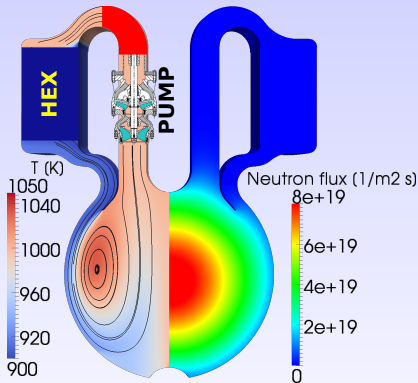
    ...

    return f;
}
```



Application: MSFR reactivity insertion

Investigate the effect of fluid compressibility



- Fuel salt expansion is the main reactivity feedback
- Doppler is also important
- Density change is limited by the speed of sound
- 1300 m/s (pure liquid)
600 m/s (Gas bubbles)
- In fast transients speed of sound is relatively small: thermal-expansion is not in equilibrium with temperature fields

Modelling conditions “close” to GODIVA super prompt-critical transients

Compressible sonic solver

Linearized momentum equation and continuity equation

$$\rho \frac{\partial \mathbf{U}}{\partial t} = \nabla (\rho \mathbf{U} \cdot \mathbf{U}) + \mu \nabla^2 \mathbf{U} = -\nabla p \quad (4)$$

```
fvm::ddt(rho,U) + fvm::div(phi,U) + fvm::laplacian(mu,U) = - fvc::grad(p)
```

$$\frac{\rho}{\partial t} = -\nabla (\rho \mathbf{U}) \quad (5)$$

```
fvm::ddt(rho) = + fvc::div(phi)
```

Linearized equation of state

$$\rho = \rho_0 + \psi (p - p_0) - \rho_0 \beta (T - T_0) \quad (6)$$

Compressible sonic solver

Pressure equation

$$\psi \frac{\partial p}{\partial t} + \nabla (\rho \mathbf{U}) = \rho_0 \beta \frac{\partial T}{\partial t} + \dots \quad (7)$$

```
fvm::ddt(psi, p) + fvc::div(phi) = fvc::ddt(rho_0 * beta, T) + ...
```

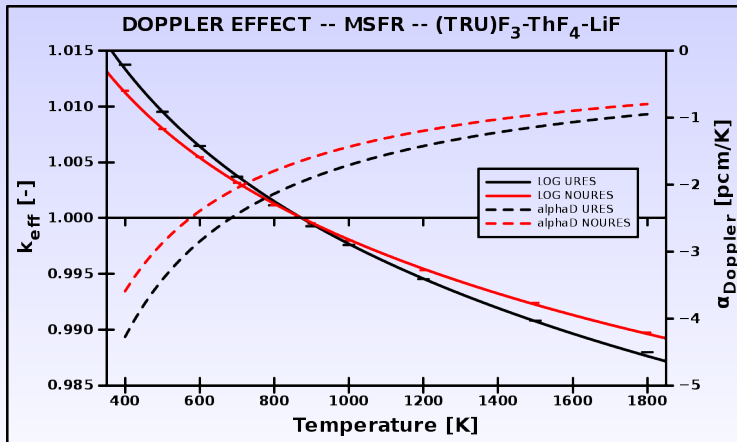
Energy equation

$$\rho c_p \frac{\partial T}{\partial t} + \rho c_p \nabla (\rho T) - \rho c_p \alpha \nabla^2 T = q''' \quad (8)$$

```
fvm::ddt(rho * c_p, T) + fvm::div(phi * c_p, T) - fvm::laplacian(rho * c_p *  
alpha, T) = volPower
```

Doppler effect: RESOLVED and UNRESOLVED resonances broadening

Logarithmic material interpolation



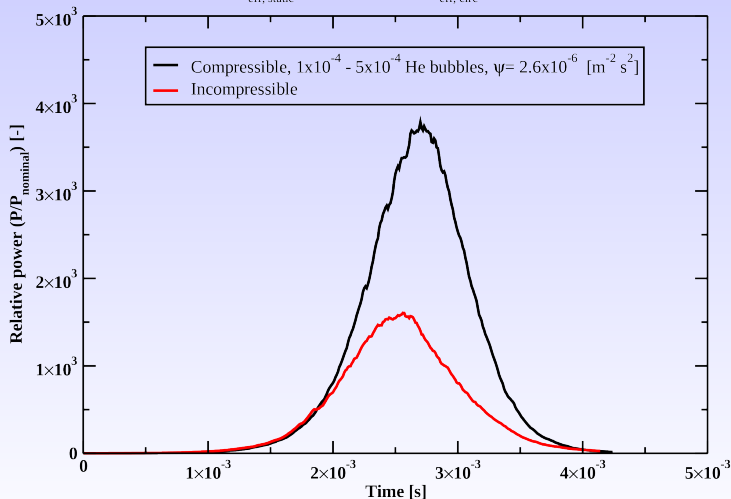
MSFR super prompt-critical burst

Effect of fluid compressibility – TRU started MSFR

Prompt reactivity insertion from zero power: ~ 230 pcm

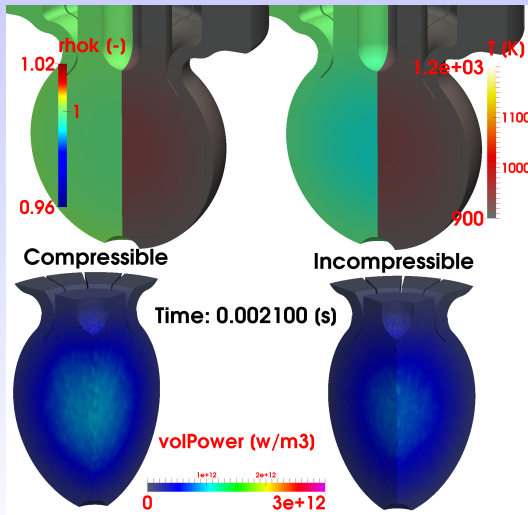
$\beta_{\text{eff, static}} \sim 300$ pcm

$\beta_{\text{eff, circ}} \sim 145$ pcm



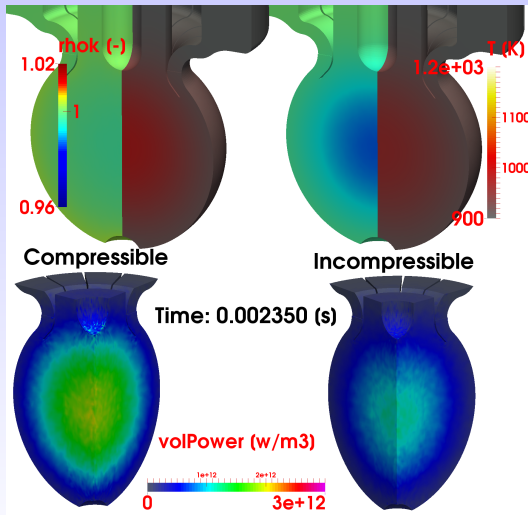
MSFR super prompt-critical burst

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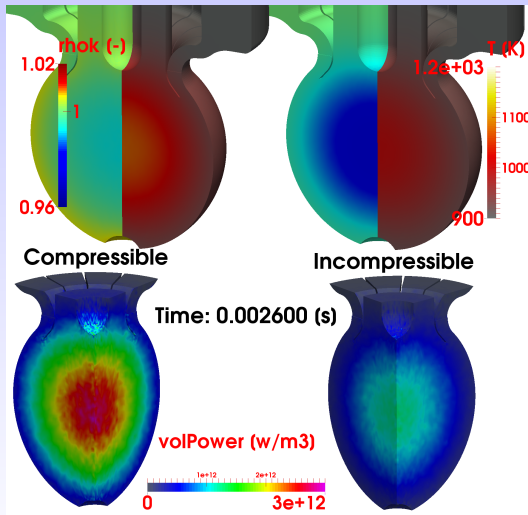
MSFR super prompt-critical burst

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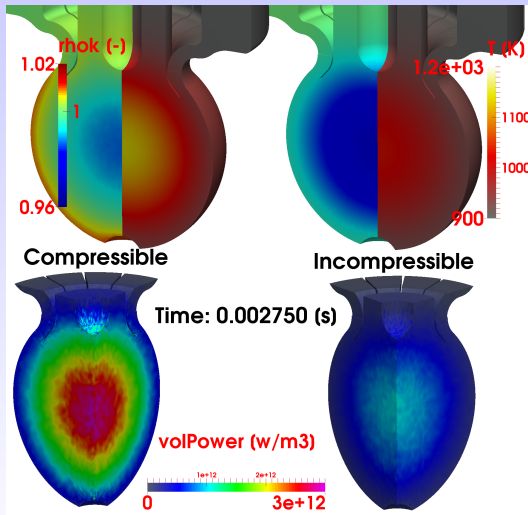
MSFR super prompt-critical burst

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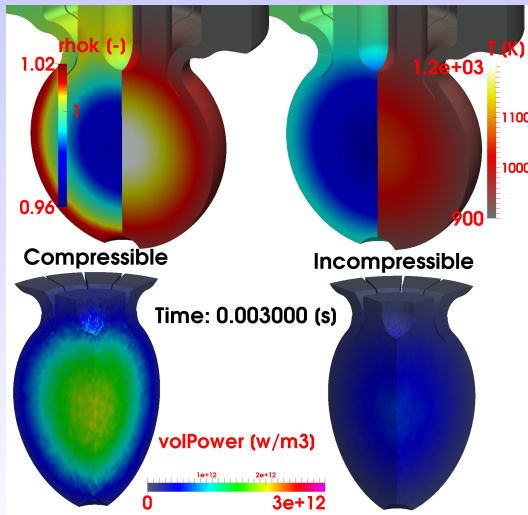
MSFR super prompt-critical burst

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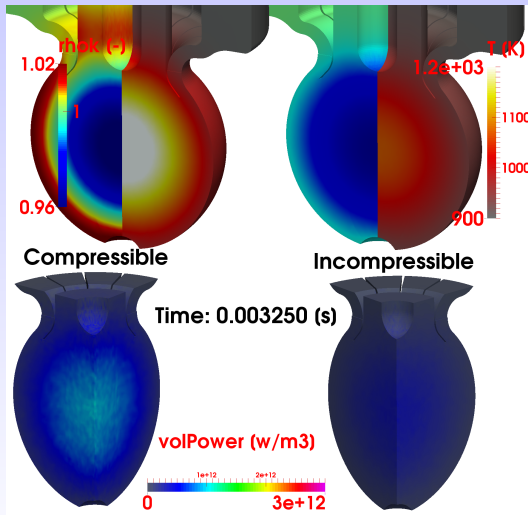
MSFR super prompt-critical burst

Effect of fluid compressibility – TRU started MSFR



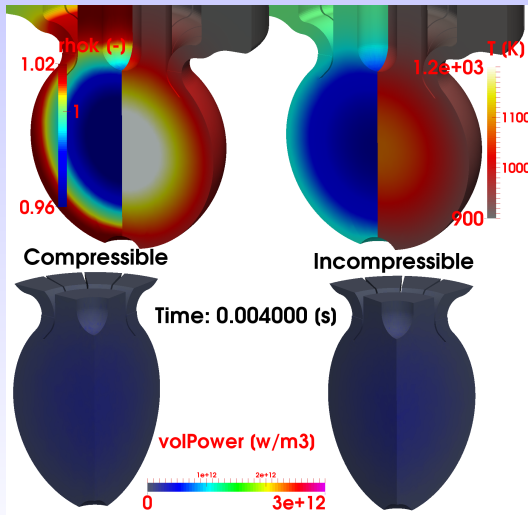
MSFR super prompt-critical burst

Effect of fluid compressibility – TRU started MSFR



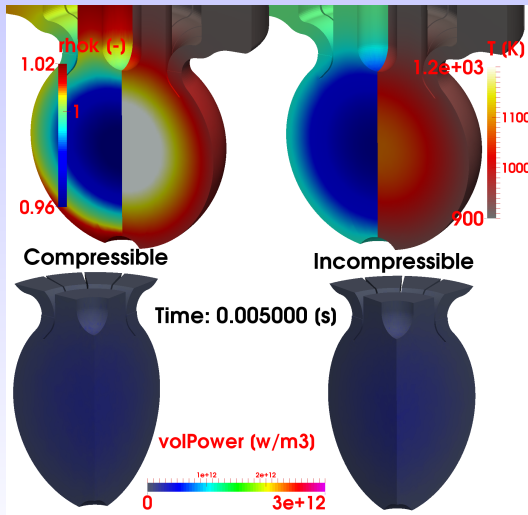
MSFR super prompt-critical burst

Effect of fluid compressibility – TRU started MSFR

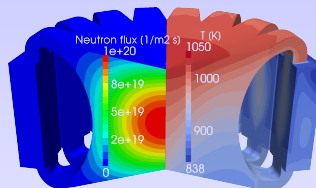
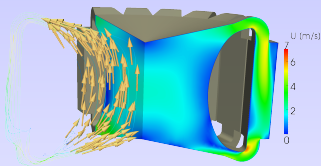


MSFR super prompt-critical burst

Effect of fluid compressibility – TRU started MSFR



Simulation tools for the MSFR



- Legacy reactor physics codes are not suitable for MSFR steady-state and transient analysis
- (Unfortunately) the development of new tools is required
- These new tools should be tested/verified/compared

Code development in the EVOL project

Several multiphysics tools have been developed, adopting a variety of approaches:

- Neutronics
 - Deterministic (mainly few-group diffusion)
 - Monte Carlo
 - Hybrid (e.g., fission matrix)
- Spatial-discretization
 - Finite-volume
 - Finite-element
 - ...
- Time-integration/coupling
 - Explicit
 - Implicit (Euler, BDF, RK, ...)



Code development in the EVOL project

- Code availability
 - Open source-based (e.g., OpenFOAM, SERPENT, ...)
 - In-house (POLIMI, TUDelft, KIT Karlsruhe, ...)
 - Commercial (COMSOL, FLUENT, ...)
 - 2D (r, z ,) codes
 - Fully 3D codes
 - Parallel computing capabilities ?

How should we test/verify/compare the different tools?



How should we test/verify/compare the different tools?

The problem

Results of the EVOL CFD benchmark and comparisons among the partners highlighted differences for steady-state and transient simulations.

Several suspects have been identified:

- Nuclear data libraries
- Delayed neutrons data
- Turbulence models
- Geometrical domain approximations
- Coarse mesh discretization
- ...

Impossible to verify the consistency of the results of the different tools!



Simplified benchmark for MSFR simulation tools

Focus only on multiphysics coupling

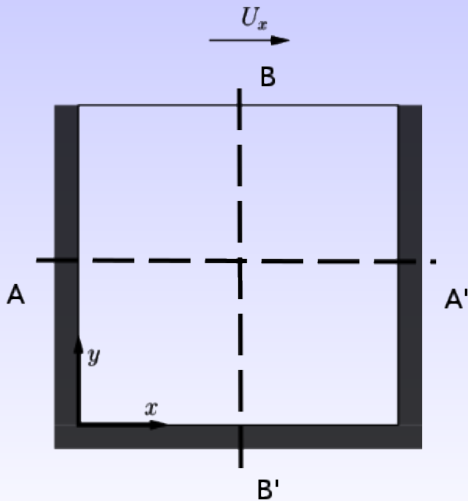
Let's get rid of any OTHER source of discrepancies:

- Simple 2D geometry
- No turbulence (laminar solution)
- Cartesian spatial discretization



Simplified benchmark for the MSFR simulation tools

Simple geometry



Simplified benchmark for the MSFR simulation tools

Material composition:

- Flibe ($\text{LiF} + \text{BeF}_2$ at 2:1). Natural Li enrichment
- ^{235}U as fissile

High neutronics similarity with the MSFR in terms of:

- Reaction rates ratios (similar neutron spectrum)
- k_{inf} , dominance ratio



Simplified benchmark for MSFR simulation tools

Phase-0 Single-physics verification

Step-0.1 Velocity field

Step-0.2 Neutronics

Step-0.3 Temperature field

Phase-1 Steady-state coupling

Step-1.1 Circulating fuel

Step-1.3 Power coupling

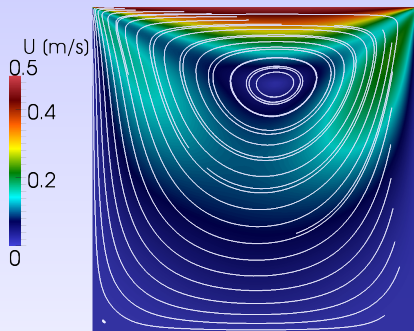
Step-1.5 Buoyancy

Step-1.7 Full coupling

Phase-2 Transient simulations



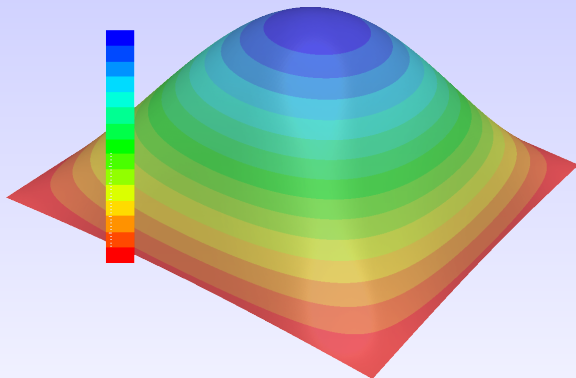
Step-0.1 Velocity field



Velocity U_x imposed at the top boundary of the square 2D cavity.
Viscosity increased to have stable laminar solution.

Step-0.2 Scalar neutron flux distribution

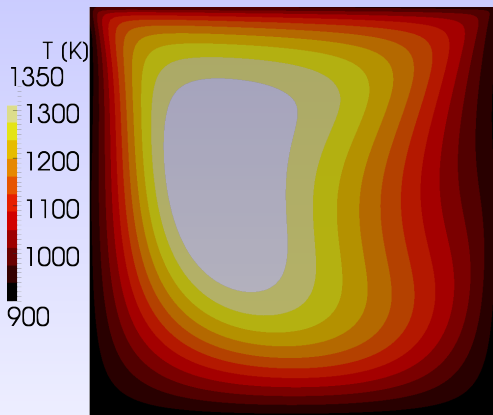
Scalar Neutron Flux (a.u.)



Vacuum boundary conditions.

Very small spectrum change from the center to the boundaries.

Step-0.3 Temperature field



Heat source distribution from Step-0.1.

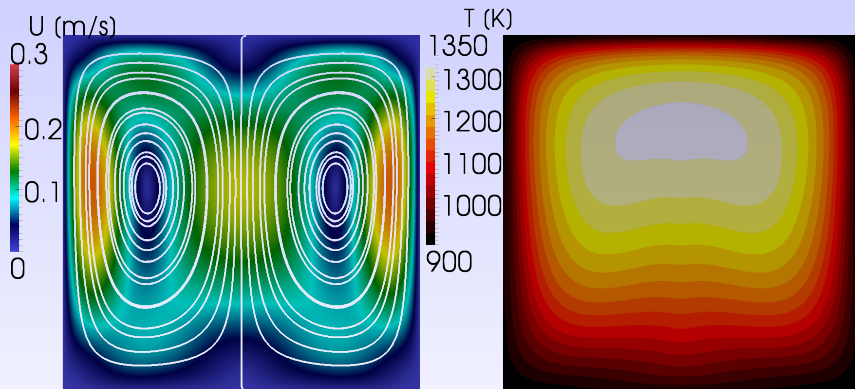
Velocity field from Step-0.2.

$$q'' = h \cdot (T - T_{cold}) \quad T_{cold} = 900K.$$

Thermal conductivity $1 \text{ W/m} \cdot K$.

Step-1.1 “Buoyancy” (two-way coupling)

Temperature and velocity fields

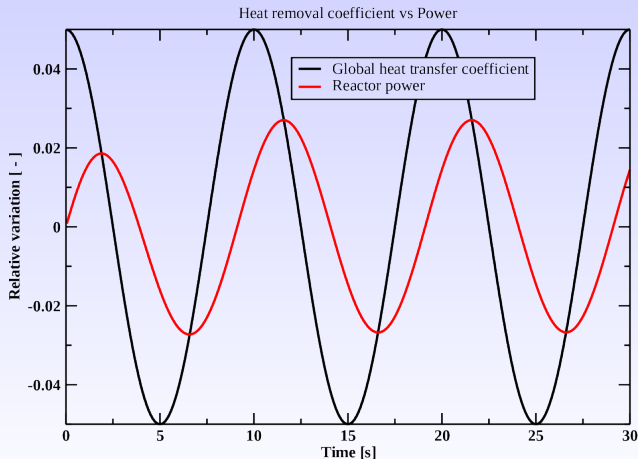


Constant fuel volumetric expansion coefficient ($2 \cdot 10^{-4} K^{-1}$).

Phase-2 Transient simulation

Still under definition

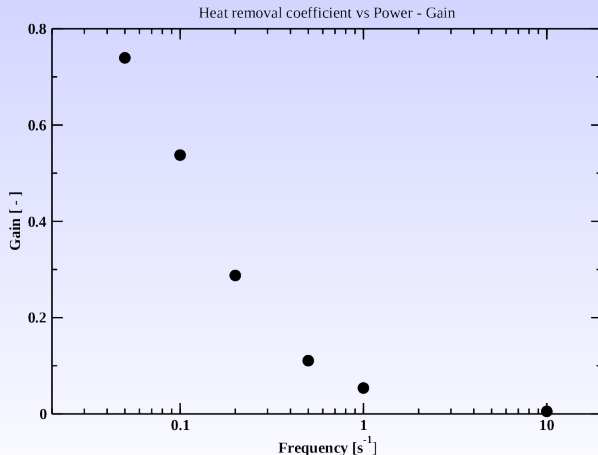
Verification of the system response to periodic perturbations.
MSRs benchmark. Transient simulations.



Phase-2 Transient simulation

Still under definition

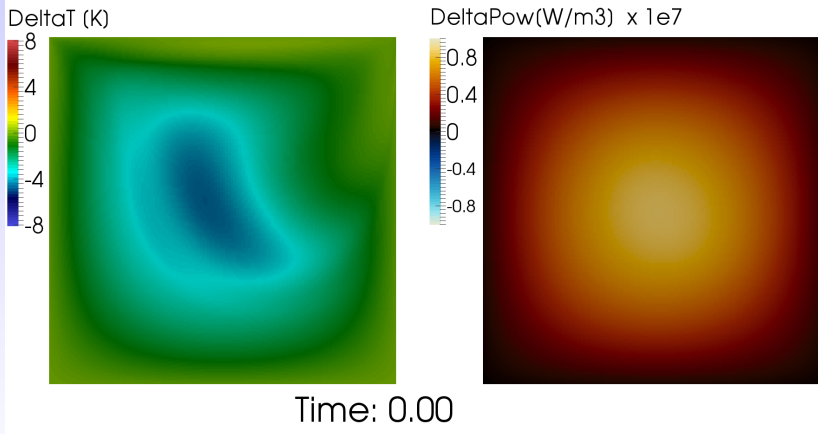
Verification of the system response to periodic perturbations.
MSRs benchmark. Periodic perturbation.



Phase-2 Transient simulation

Still under definition

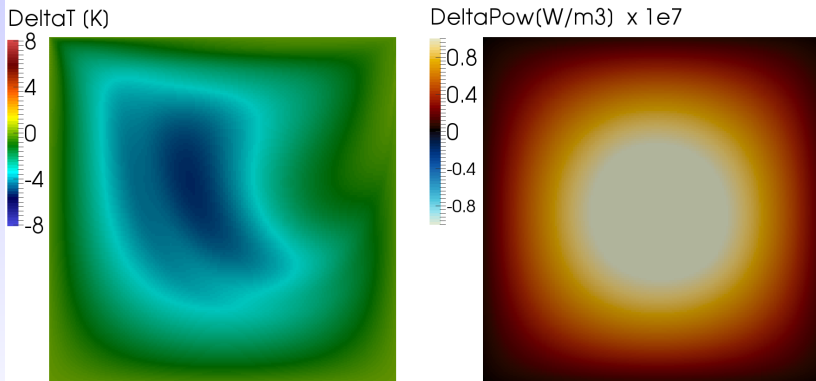
Verification of the system response to periodic perturbations.



Phase-2 Transient simulation

Still under definition

Verification of the system response to periodic perturbations.

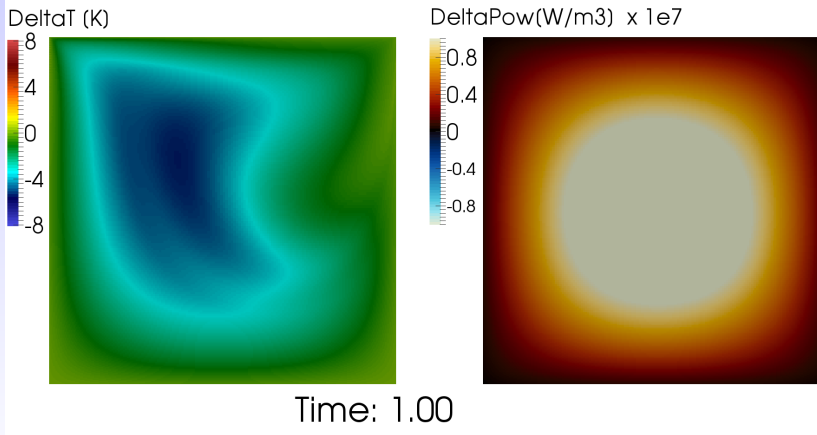


Time: 0.500

Phase-2 Transient simulation

Still under definition

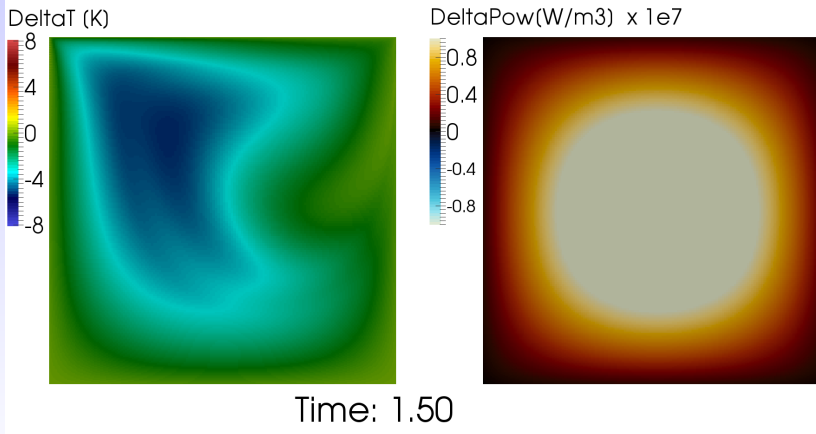
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Phase-2 Transient simulation

Still under definition

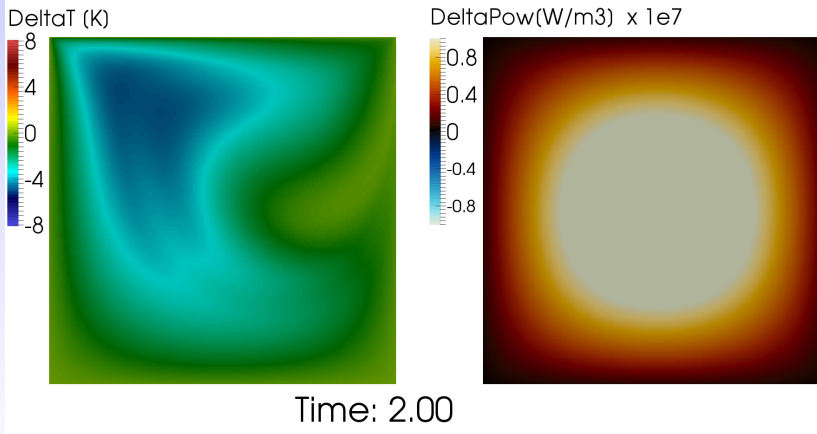
Verification of the system response to periodic perturbations.



Phase-2 Transient simulation

Still under definition

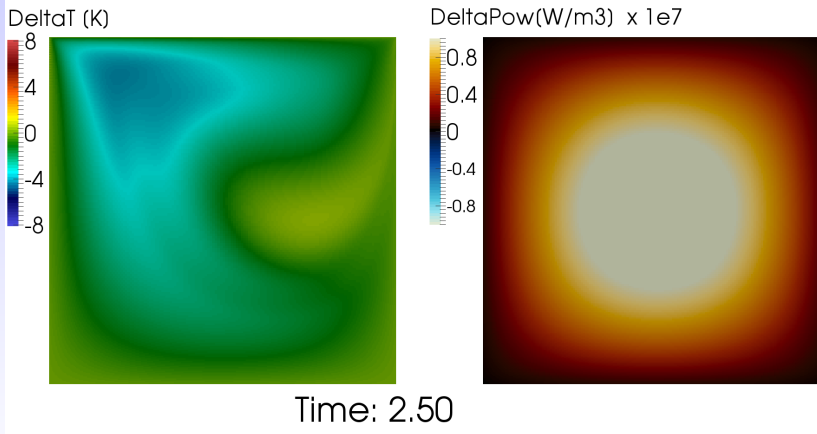
Verification of the system response to periodic perturbations.



Phase-2 Transient simulation

Still under definition

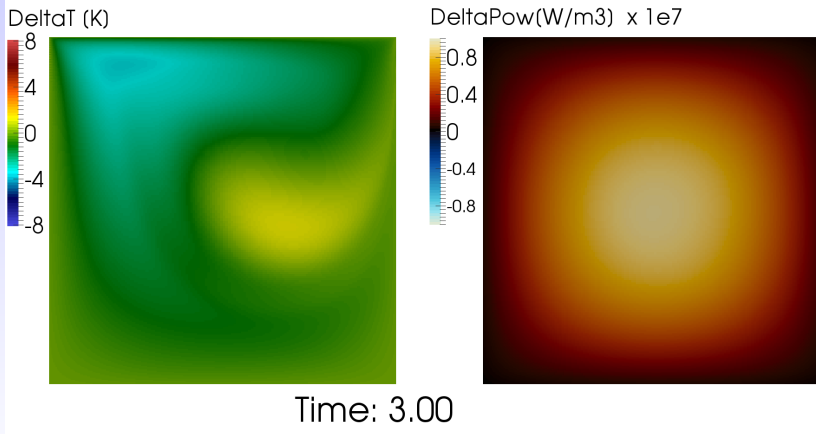
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Phase-2 Transient simulation

Still under definition

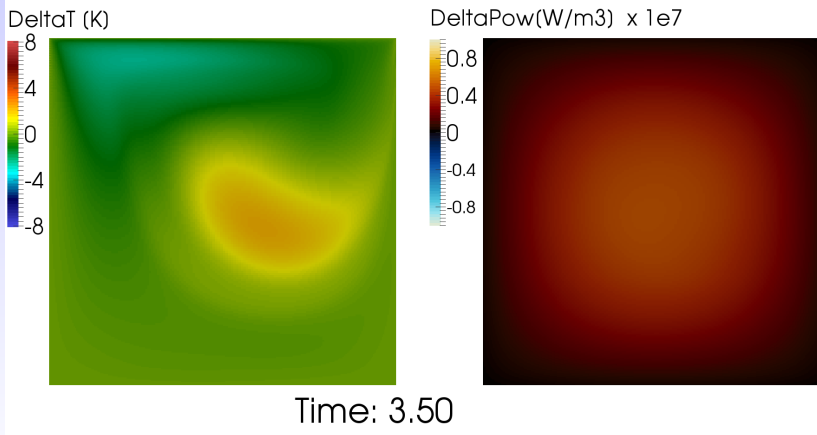
Verification of the system response to periodic perturbations.



Phase-2 Transient simulation

Still under definition

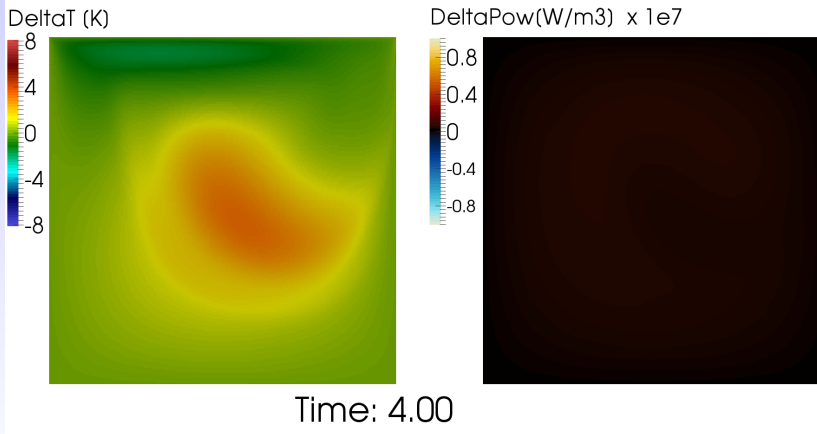
Verification of the system response to periodic perturbations.



Phase-2 Transient simulation

Still under definition

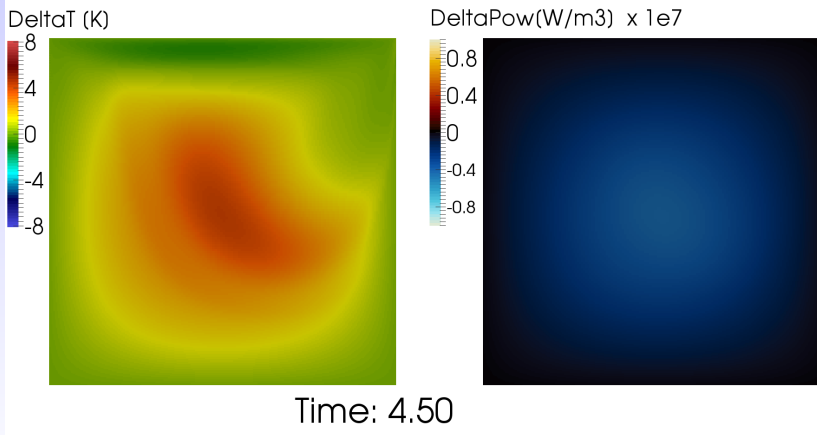
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Phase-2 Transient simulation

Still under definition

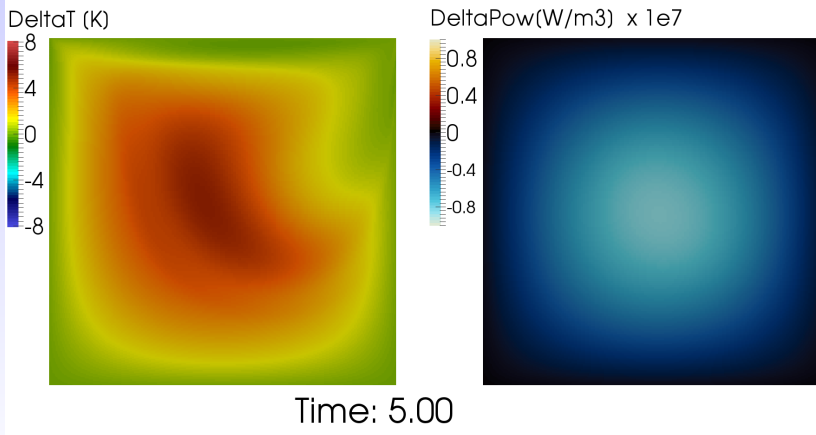
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Phase-2 Transient simulation

Still under definition

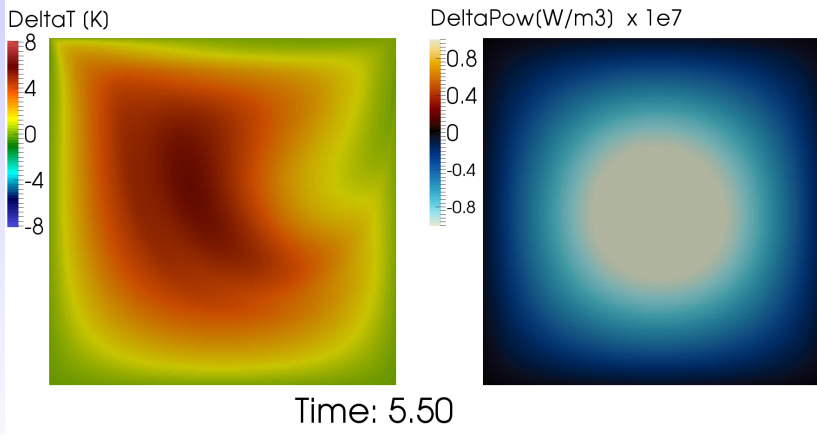
Verification of the system response to periodic perturbations.



Phase-2 Transient simulation

Still under definition

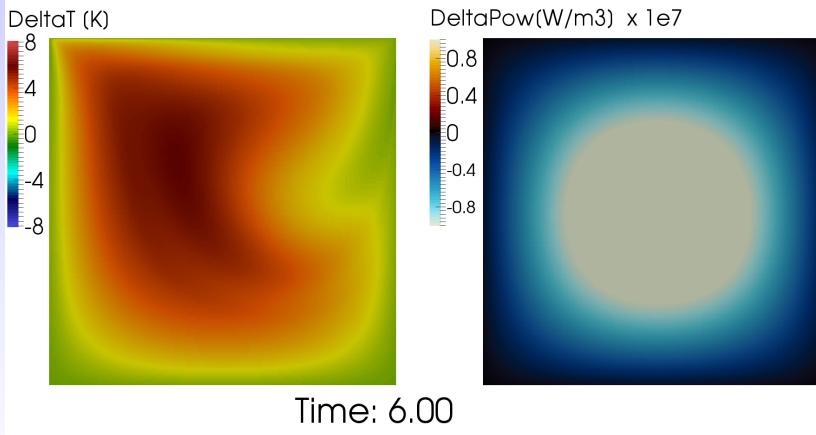
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Phase-2 Transient simulation

Still under definition

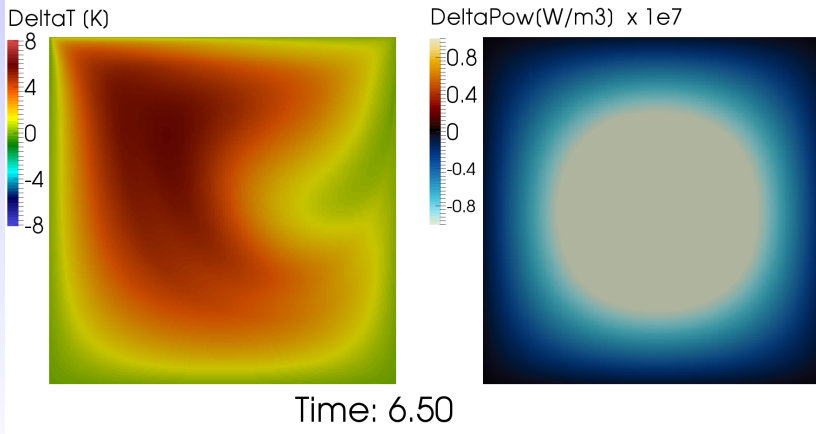
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Phase-2 Transient simulation

Still under definition

Verification of the system response to periodic perturbations.

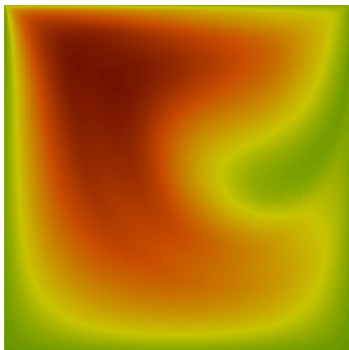
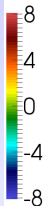


Phase-2 Transient simulation

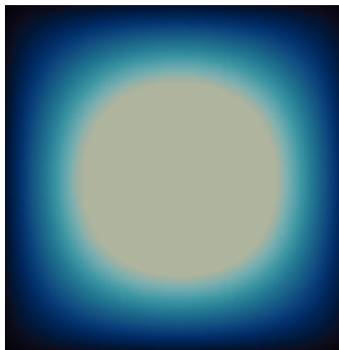
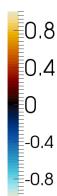
Still under definition

Verification of the system response to periodic perturbations.

DeltaT (K)



DeltaPow(W/m3) x 1e7

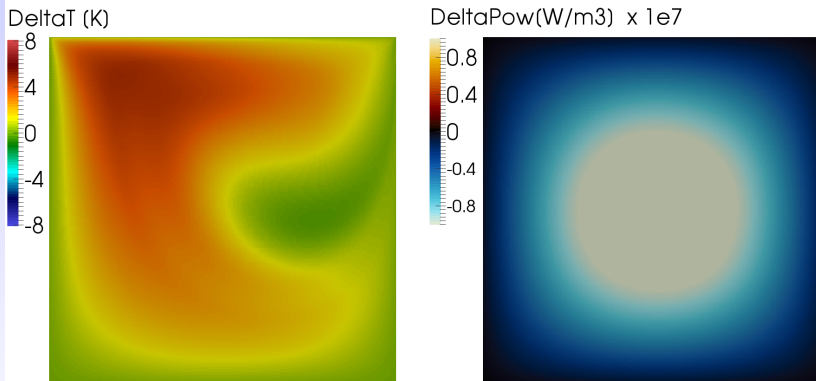


Time: 7.00

Phase-2 Transient simulation

Still under definition

Verification of the system response to periodic perturbations.

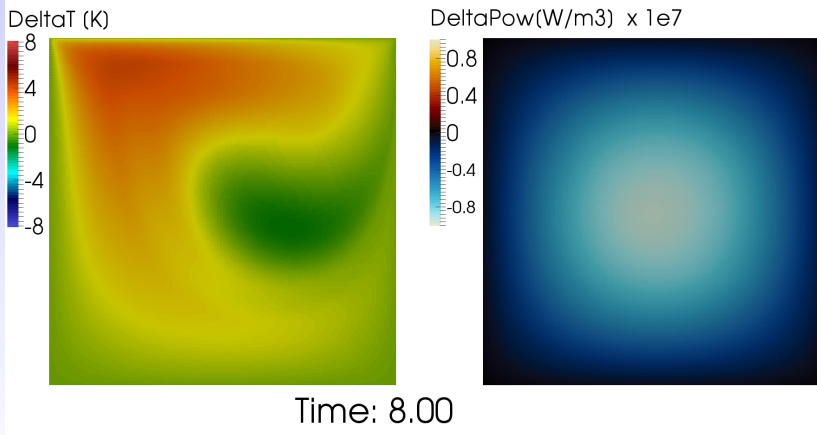


Time: 7.50

Phase-2 Transient simulation

Still under definition

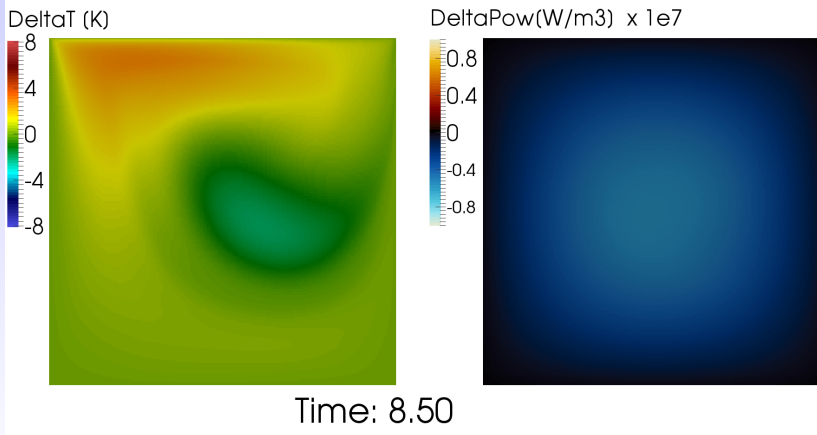
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Phase-2 Transient simulation

Still under definition

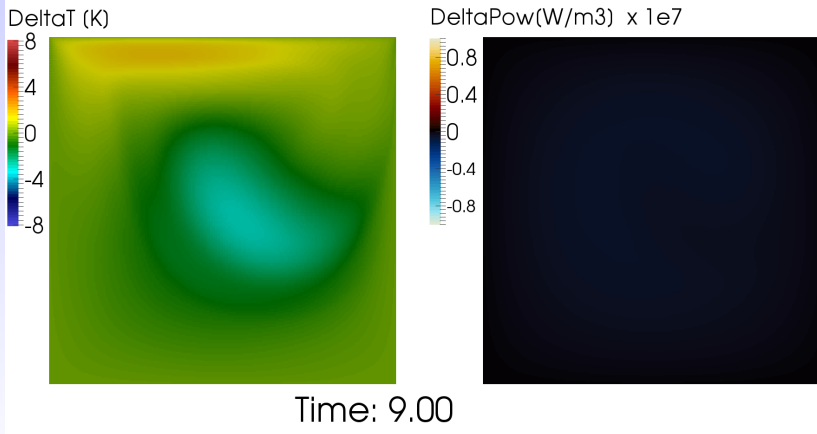
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Phase-2 Transient simulation

Still under definition

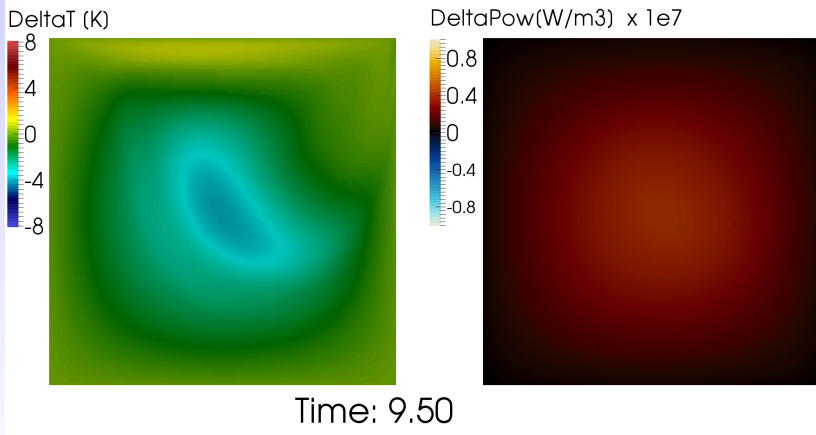
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Phase-2 Transient simulation

Still under definition

Verification of the system response to periodic perturbations.

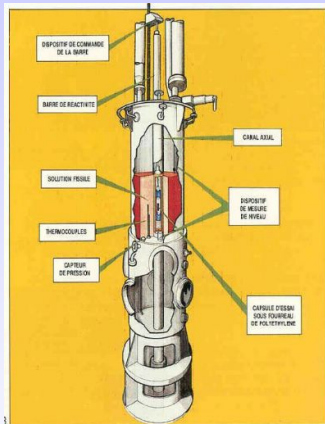


Conclusions (Serpent–OpenFOAM)

- Serpent-OpenFOAM proved to be quite useful for criticality accident modelling
- We are considering other validations against experimental data (SILENE reactor)...
any suggestions?



Silene reactor



3

Next steps (Serpent–OpenFOAM)

- Volume-integrate approach (analog/implicit) for delayed neutron precursors
- Extension of the approach to other physics and reactors
- Long term goal: uncertainty propagation with Generalized Perturbation theory in Serpent–OpenFOAM



Acknowledgement

- Mathieu Salanne (Université Pierre et Marie Curie)
molecular dynamics calculation
 $LiF-ThF_4$ bulk modulus
- Serpent team



Conclusions (MSRs benchmark)

- A simplified benchmark is under definition
- Focused on multiphysics coupling
- Ideal for reduced order modelling tools
- Reference results from Serpent simulations
- Anyone interested?



THANK YOU FOR THE ATTENTION



QUESTIONS? SUGGESTIONS? NEW IDEAS?