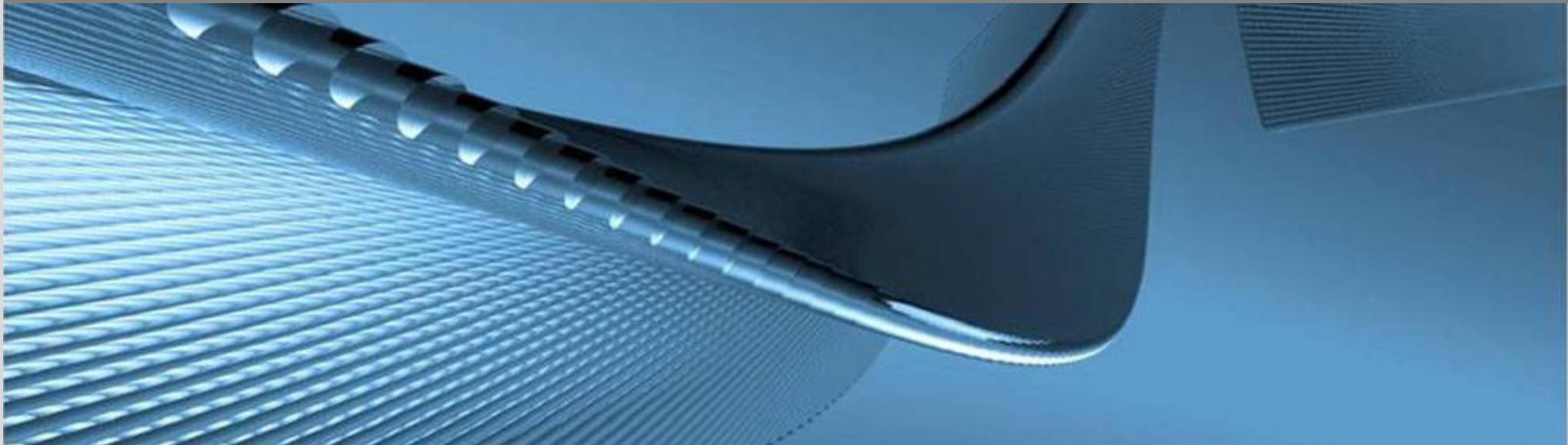


Overview of KIT activities on fuel cycles options for phase-out and regional scenarios

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- The CAPRA/CADRA project
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- Summary

Nuclear fuel cycle and transmutation studies at KIT

The **KIT (IKET/TRANS group)** is **involved** in fuel cycle and transmutation studies since long time. An overview of the main projects and findings is reported in the following slides.

The activities have been grouped as follows:

- Activities related to the **CAPRA / CADRA Project** (assessment of Pu burner system)
- Activities related to the **FP6 – PATEROS Project** (P&T on regional scenario studies)
- The **German P&T study** (2012-2014)
- Activity (on-going) on **burner systems characterizations for waste minimization**

The **KIT (IKET-TRANS group)** is participating to the **OECD/NEA EG in Advanced Fuel Cycle Scenario studies**.

The code used at KIT for scenario studies is **COSI6 code** (CEA). For each system considered, **reactor-dependent libraries are generated at KIT (IKET-TRANS group)** by means of **ECCO/ERANOS** code.

The CAPRA / CADRA Project

The CAPRA / CADRA Project

The **joint European CAPRA / CADRA program** launched by CEA (France) in early '90s → investigations of critical reactors for **transmutation and incineration of nuclear waste**. The IKET-TRANS group was extensively involved in **safety studies**.

The **CAPRA** (Combustion Améliorée du Plutonium dans les Réacteurs Avancés) mainly deals with **managing the plutonium stockpile** and **CADRA** (Consommation d'Actinides et de Déchets dans les Réacteurs Avancés) is related to the **burning/transmutation of MAs and LLFPs**. The CAPRA / CADRA program comprises **the development of advanced LWRs, FRs, with different coolants and ADS**.

The originally designed CAPRA / CADRA core was planned to be **the size of a conventional FR** as the European Fast Reactor (EFR) core (1300 MWe).

Reversibility in this case **meant that a plant, such as the EFR, may host core with BR>1 (reference EFR core) and CAPRA / CADRA core for burning plutonium and MAs during the life of the plant without requiring any changes to be made in plant design.**

The FP-6 PATEROS Project

The FP-6 PATEROS Project

The **FP6 - PATEROS project** (coordinated by SCK-CEN – 2006 -2008) → establishing a European vision for the deployment of P&T of Nuclear Waste, up to the level of industrial implementation → **regional scenario**.

The **possibilities to share fuel cycle facilities have been investigated** within the project. It is envisaged a concerted use of materials, in order to optimize the use of resources and investments in an enhanced proliferation resistant environment.

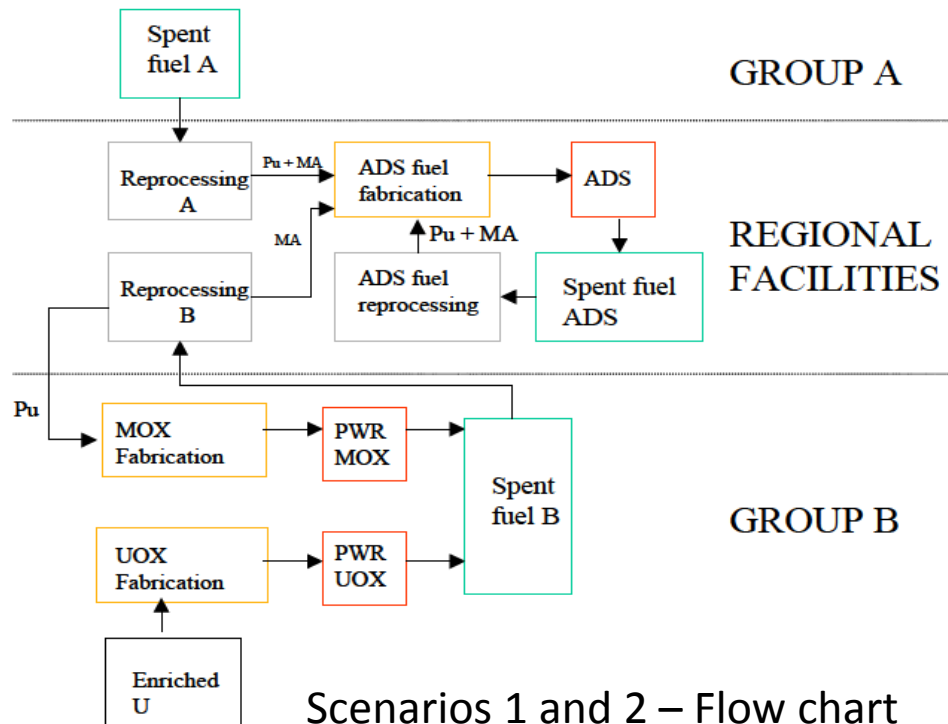
European situation has been analyzed by considering four groups of countries:

- Group A is in a **stagnant or phase-out scenario** (e.g. Germany) for nuclear energy and has to manage his spent fuel, and especially the plutonium and the minor actinides.
- Group B is in a **continuation scenario** (e.g. France) for the nuclear energy and has to optimize the use of his resources in Plutonium for the future deployment of fast reactors or ADS.
- Group C (a subset of Group A), after stagnation, envisages a nuclear “renaissance”.
- Group D, initially with no NPP, decides to go nuclear.

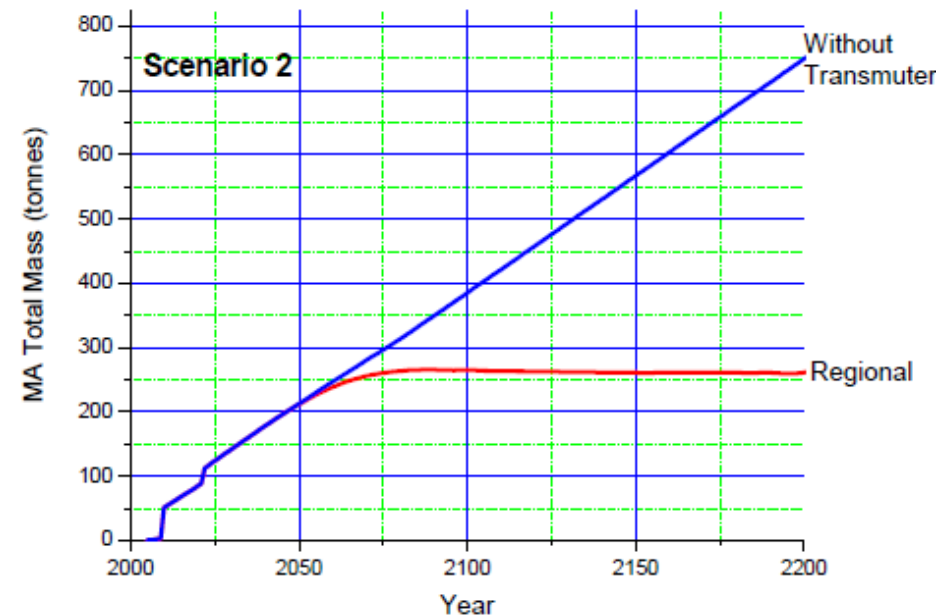
The FP-6 PATEROS Project

Mainly 3 scenarios have been selected and investigated:

- Scenarios 1 and 2 consider the deployment of a group of **ADS-EFIT** shared by countries A and B. The **ADSs use the plutonium of Group A and transmute the Minor Actinides (MA) of the two groups.**
- Scenario 3 considers the deployment of **Fast Reactors** in Group B. These **Fast Reactors use the Pu of Groups A and B and recycle all MA.**



Scenarios 1 and 2 – Flow chart



MOX in PWR

The German P&T study (2012-2014)

The German P&T study (2012-2014)

In order to identify potential advantages that **P&T** may offer for waste management strategy **in Germany**, the Federal Ministry of Economics and Technology (BMWi) and the Federal Ministry of Education and Research (BMBF) launched and granted in the period 2012-2014 an interdisciplinary research project, **to support the decision on merit of P&T implementation**.

Several **scenarios** in a **nuclear phase-out context** have been investigated:

- **Scenario 1**: no actions in support of P&T strategy
- **Scenario 2**: only R&D activities related to P&T (i.e. postponing the decision of P&T implementation)
- **Scenario 3**: Isolated application of P&T in a phase-out context.
- **Scenario 4**: Implementation of P&T in a regional (e.g. European) context.

Several **technological** options were considered:

- TRU in **U-free matrix** (MgO, Mo, ...) → **ADS – EFIT-like**
- TRU in **U matrix** → **Low CR FRs – ASTRID-like**

O. Renn, (2014), „Partitionierung und Transmutation. Forschung Entwicklung Gesellschaftliche Implikationen (acatech STUDIE)“, München, Herbert Utz Verlag.

C. Fazio, et al. „Study on partitioning and transmutation as a possible option for spent fuel management within a nuclear phase-out scenario“, Proc. Int. Conf. GLOBAL 2013, 2013.

A. Rineiski, et al. „Options for Incineration of Trans-Uranium Elements from German Spent Nuclear Fuel“, Proc. Int. Conf. ICENES2013, 2013.

The German P&T study (2012-2014)

- **Scenario 1:** no actions in support of P&T strategy
- **Scenario 2:** only R&D activities related to P&T

SNF has been produced in Germany since 1969 (LWRs-UOX and LWRs-MOX systems). According to the German phase-out schedule (abrupt shut down of 8 LWRs after Fukushima accident) the operation of the remaining 9 units will be terminated latest in 2022.

Inventory (2075)

Amount given in tons	SNF	Vitrified Waste
U	9710	0.7
Fission Products (FPs)	416	207.0
Pu	137	0.3
MA	38	4.0
TRU (Pu+MA)	175	4.3
Total (U+FPs+TRU)	10300	212.0

Fine characterization of German wastes and SNF inventories has been performed in the study*.

O. Renn, (2014), „Partitionierung und Transmutation. Forschung Entwicklung Gesellschaftliche Implikationen (acatech STUDIE)“, München, Herbert Utz Verlag.

(*) A. Schwenk-Ferrero, “German Spent Nuclear Fuel Legacy: Characteristics and High-Level Waste Management Issues”. In: Hindawi Publishing Corporation, Science and Technology of Nuclear Installations, Nr. 2013 ID 293792, 2013. URL: <http://dx.doi.org/10.1155/2013/293792> [Stand: 23. 09. 2013].

The German P&T study (2012-2014)

- Scenario 3 -4: P&T implementation**

	EFIT-like		ASTRID-like	
Matrix	MgO	Nat. Mo	UO ₂	UO ₂
Pu/MA	68/32	80/20	66/34	95/5
TRU vol%				
inner core	21	22	33	25
mid core	27	28	--	--
outer core	31	32	36	27
Power MWth	400		1200	
CR	0	0	0.55	0.68
Initial core inventory, kg				
TRU	4133	4417	6580	5087
Matrix	4532	9544	11408 (U)	12803 (U)
TRU transmutation rate (kg/TWhth) after 3 or 5 (EFIT or ASTRID) years of irradiation and 3 or 5 years cooling				
Pu	-21	-35	-4	-13
MA	-24	-9	-15	0
kg of burned TRUs / kg loaded TRUs after 3 or 5 years of irradiation (in EFIT or ASTRID) and 3 or 5 years cooling				
	-0.11	-0.10	-0.14	-0.13
Safety-related parameters: Doppler Constant and coolant void effect (in EFIT core or in ASTRID core and Na Plenum above), pcm				
K _D	-208	-267	-272	-571
Void effect	3033	3054	-88	-1138

Consequently, the **EFIT and ASTRID designs** have been adapted to the needs of the actual German phase-out.

EFIT-like and ASTRID-like systems have been defined able to transmuted both MAs and Pu. In particular with respect to the original systems, the fuel composition, power, and core height values have been adapted.

The scenarios have been compared by quantifying different **indicators**.

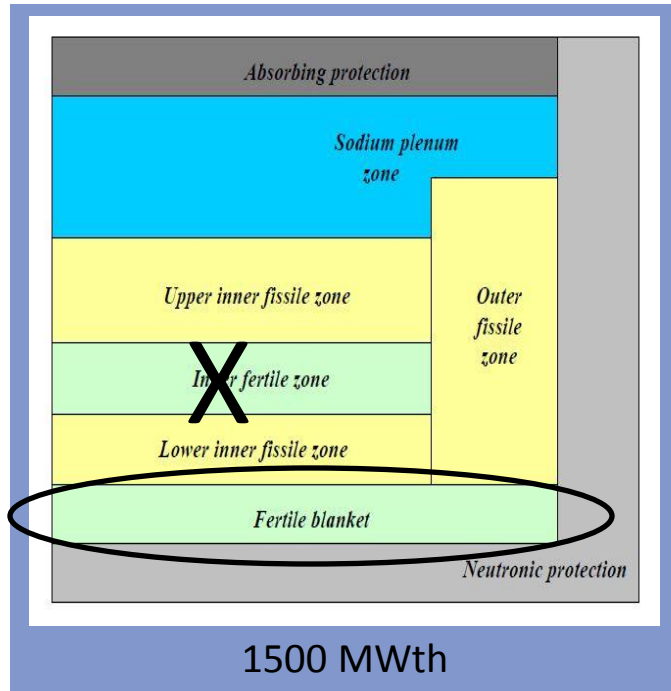
They have been then used in applying the Delphy method for assessing social opportunities and risky of P&T.

F. Gabrielli, et al. „ASTRID-like Fast Reactor Cores for Burning Plutonium and Minor Actinides”, Proc. Int. Conf. INES-4,2013.

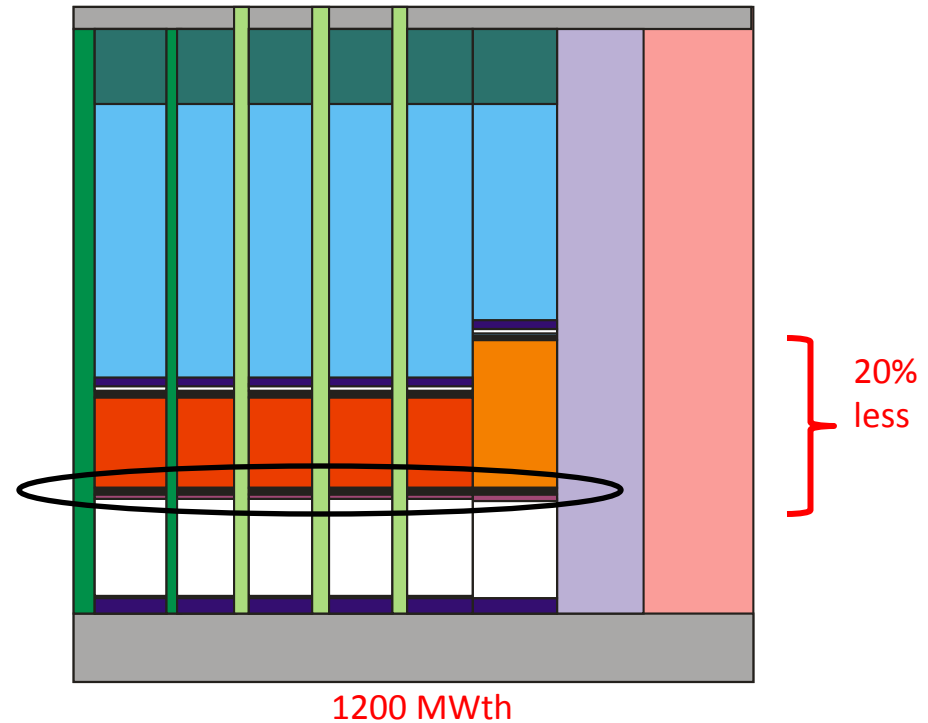
O. Renn, (2014), „Partitionierung und Transmutation. Forschung Entwicklung Gesellschaftliche Implikationen (acatech STUDIE)“, München, Herbert Utz Verlag.

Burner systems characterization for waste minimization

Burner systems characterization for waste minimization



ASTRID design (J.P. Grouiller, FR13)



ASTRID-like burner (F. Gabrielli, Energy Procedia 71, 130 – 139, 2015)

Power: 1500 MWth → 1200 MWth (20% less)

Active height: reduced by 20%

Internal fertile blanket: removed

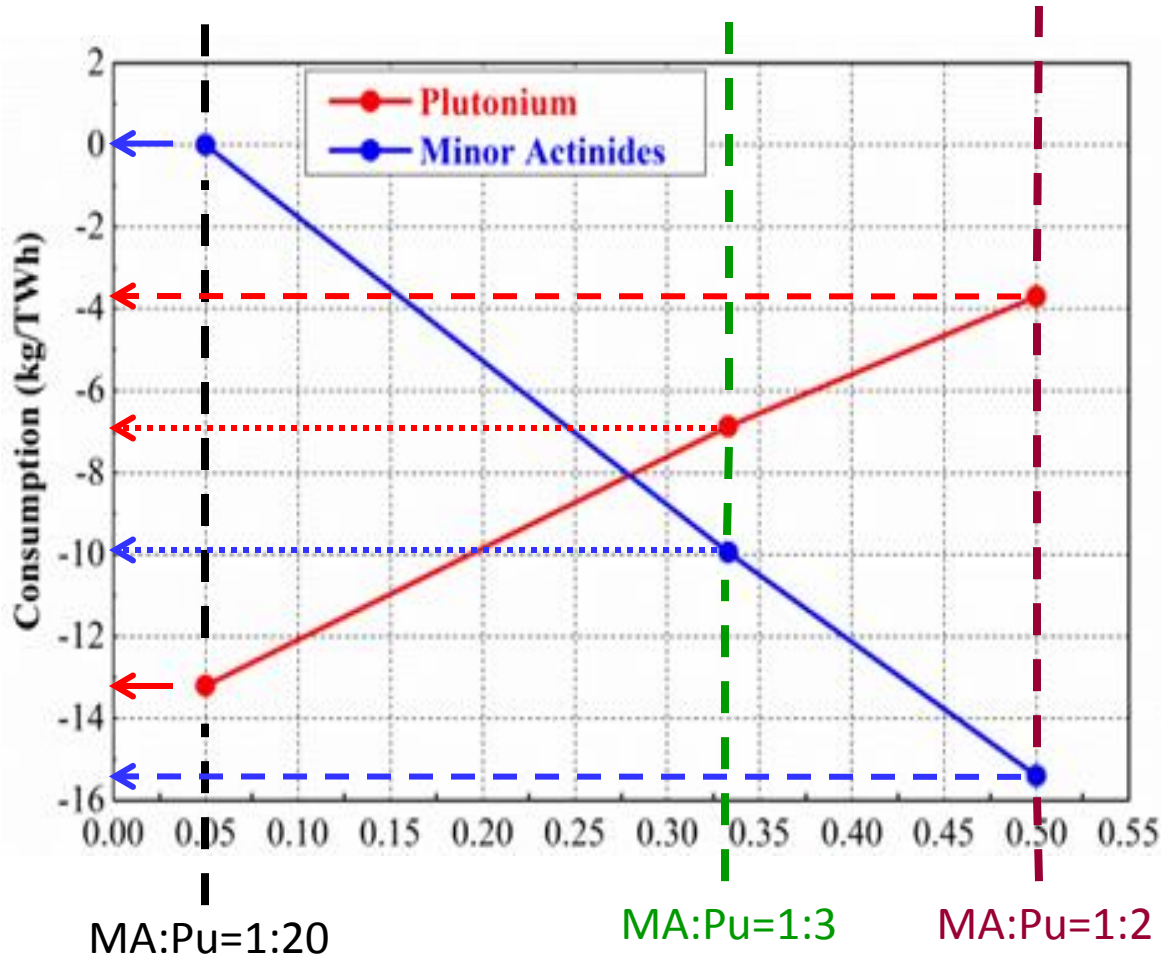
Lower fertile blanket: reduced to 2 cm

High TRU content
→ CR 0.6-0.7
(originally CR = 1)

MA:Pu contents adjusted to get the required burning rates

Burner systems characterization for waste minimization

System **flexibility** → same geometry, same power (1200 MWth) → different fuel compositions (MA:PU ratio) → target: MA/TRU burning rates to meet specific scenario needs.



MA:Pu=1:20

→ Pu burner

→ Phase-out scenarios

(Pu main component to TRU inventory, radiotoxicity, .. to be reduced at first)

MA:Pu=1:2

→ mainly MA burner

→ On-going/regional scenarios
(need to stabilize MA inventory)

Large MA content (ca. 12%) in fuel → Safety coefficients remain acceptable but deteriorate.

MA:Pu=1:3

→ mainly MA burner

→ On-going/regional scenarios

Lower MA content (ca. 8%) in fuel
→ Better safety behavior

Burner systems characterization for waste minimization

Safety performances:

Parameter	MA:Pu=1:20		MA:Pu=1:2		MA:Pu=1:3	
	BOL	EOC3	BOL	EOC3	BOL	EOC3
$\beta_{\text{eff}}(\text{pcm})$	331	328	275	272	331	328
$\Lambda(\mu\text{s})$	0.66	0.63	0.42	0.47	0.61	0.63
$K_D(\text{pcm})$	-571	-540	-275	-272	-352	-361
Reactor Condition	$\Delta\rho(\text{\$})$		$\Delta\rho(\text{\$})$		$\Delta\rho(\text{\$})$	
Voided core	3.1	4.0	5.9	6.1	4.3	4.6
Voided core + plenum	-3.4	-2.6	-0.3	-0.6	-1.2	-1.1

(F. Gabrielli, et al., Energy Procedia 71, 130 – 139, 2015)

Considered in regional scenarios

Neutron transport calculations performed by means of the **ECCO/ERANOS** code (VARIANT solver) assuming 3D (HEX-Z) models, effective XS in 33 energy-groups, JEFF3.1 nuclear data library.

Dedicated libraries for fuel cycle code **COSI6** have been generated at KIT.

For checking the full procedure (from **ERANOS** to **COSI6** core modeling) and before adding sources of “uncertainties” due to the scenario dynamic isotopic vector evolution, the **same conditions used in ERANOS simulation have been applied to COSI6**. The effect of different initial TRU vectors have also been considered.

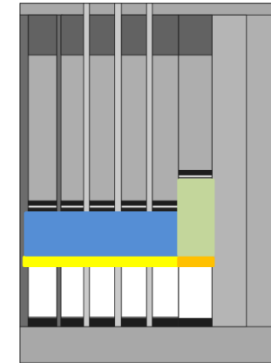
Burner systems characterization for waste minimization

Same conditions used in ERANOS simulation have been applied to COSI6:

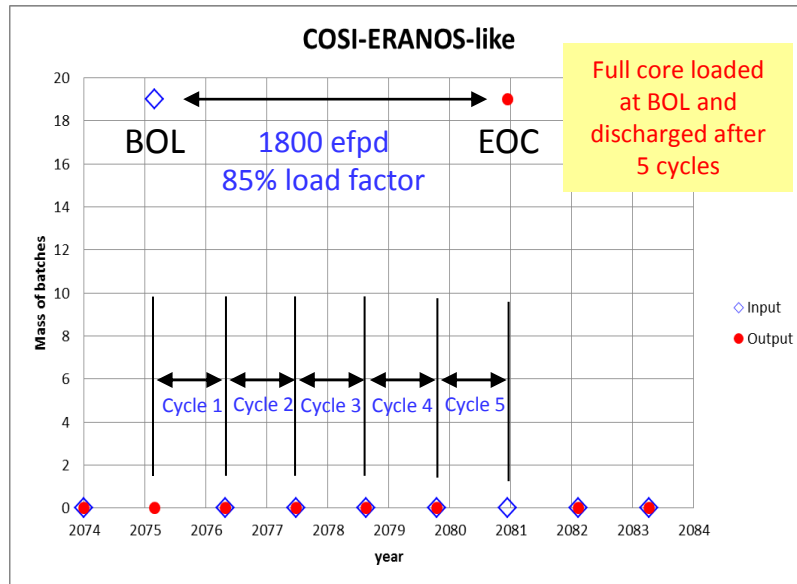
1. Full core modeled.
2. No reshuffling.
3. A single irradiation step of 1800 efpd.

System modeled by 4 BBLs.

Fuel composition loaded in core calculated by the COSI itself using Pu239eq. and omega values (BOL) from ERANOS.



	Inner core (eq. Model 1)
	Outer core (eq. Model 2)
	LAB inner zone
	LAB outer zone



MA burner		
U+TRU inventory	ERANOS	COSI6
	kg	
BOL	18601	19022
EOC	16413	16806
ΔM	2188	2216

Main difference from Pu241 burning rate

MA burner			
Elements	ERANOS	COSI6	
		As ERANOS	In scenario (eq. batch)
		kg/TWhth	
U	-23.5	-24.2	-23.7
Pu	-4.2	-3.3	-3.5
Am	-16.80	-17.32	-17.44
MA	-14.7	-15.2	-15.5

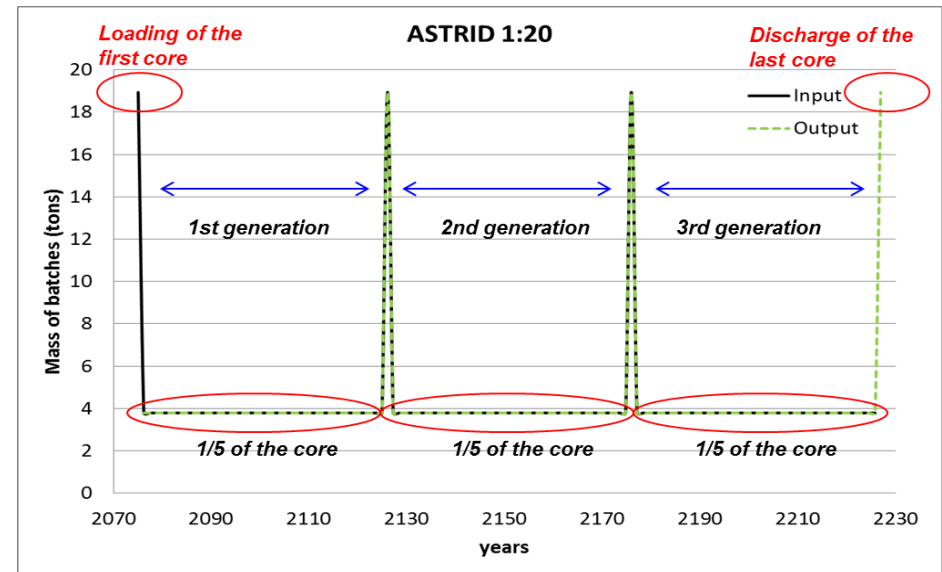
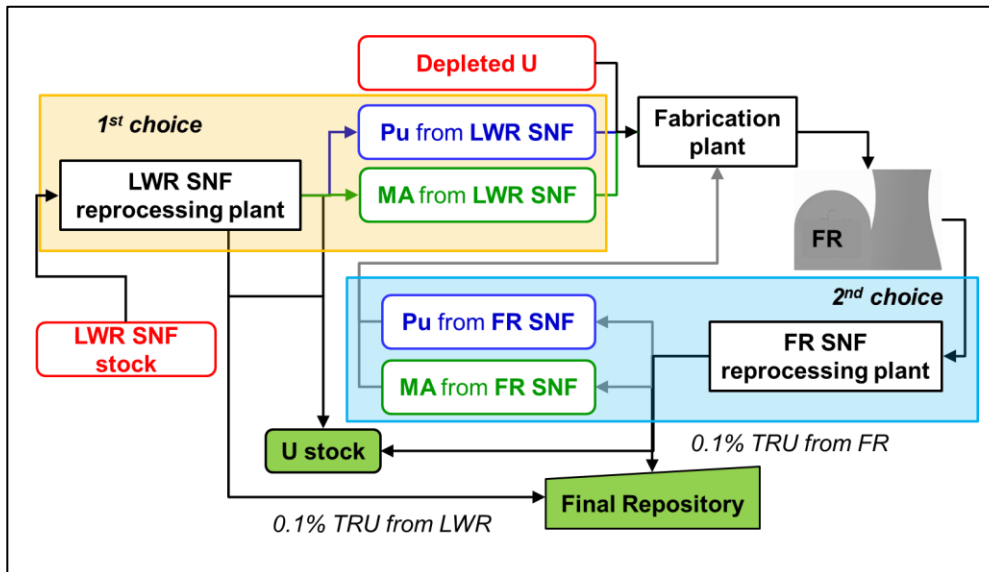
Toward phase-out scenario studies

Toward phase-out scenario studies

The **German accumulated TRU inventory** assumed to be burned in about **150 years***.

Starting **from 2075** (date arbitrary chosen) **three generations of burners** (50 years lifetime each) assumed.

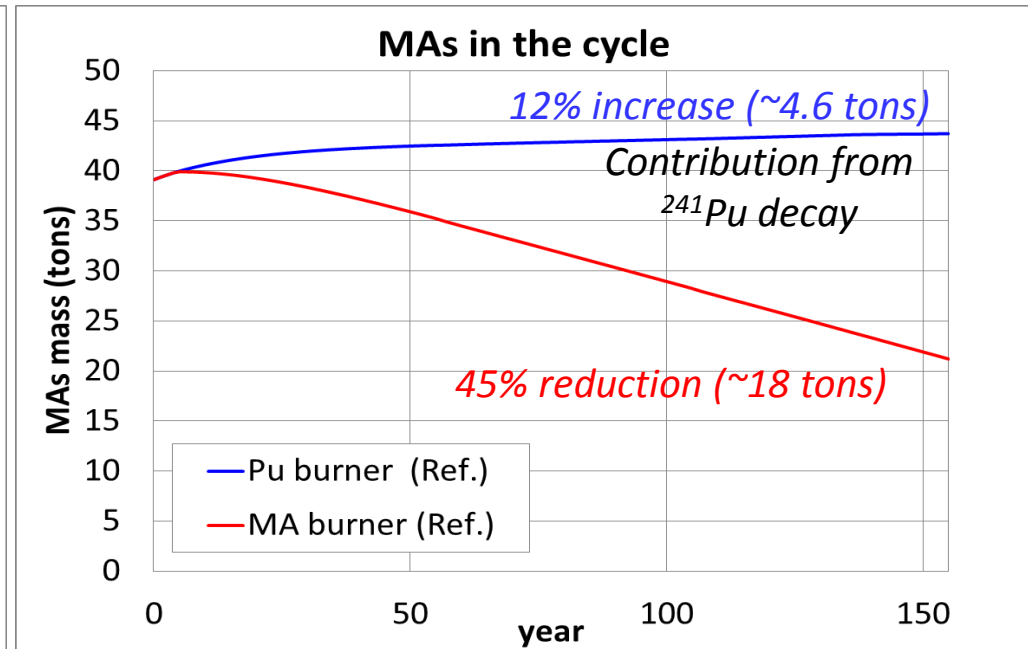
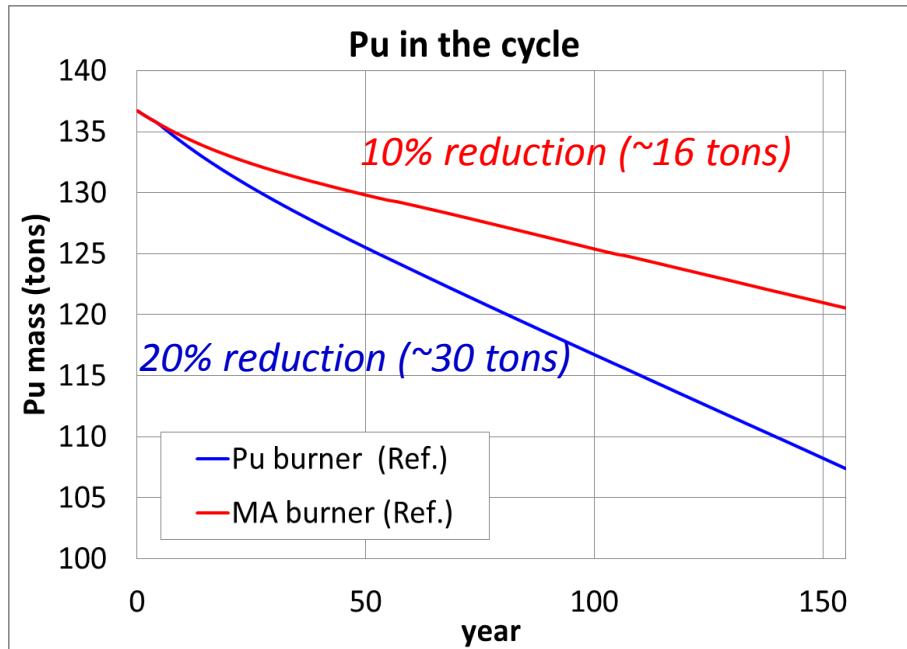
Comparison: deployment of one single unit (Pu or MA burners) → analysis of burners behavior under dynamic conditions**.



*O. Renn, (2014), „Partitionierung und Transmutation. Forschung Entwicklung Gesellschaftliche Implikationen (acatech STUDIE)“, München, Herbert Utz Verlag [conservative value adopted].

**B. Vezzoni, et al. „Minor Actinides Incineration Options using Innovative Na-cooled Fast Reactors: Impact on Phasing-out and On-going Fuel Cycles“, Progress in Nuclear Energy, Volume 82, Pages 58–63, July 2015.

Toward phase-out scenario studies

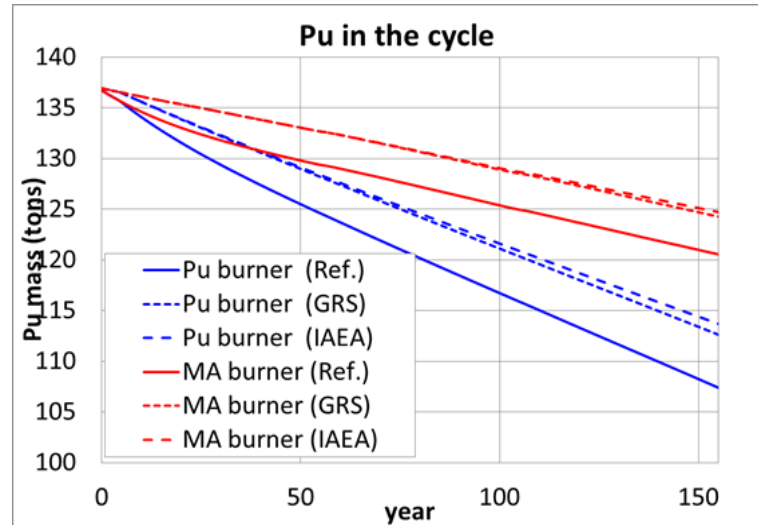


After introduction of a **single unit** → **large residual mass of TRU** remains in the cycle.

The complete TRU burning may be achieved by a fleet of about 4 to 5 Pu burners and 2 MA burners (or **6-7 systems with intermediate characteristics**) corresponding to an “effective CR” of about 0.62-0.65 → results confirm the conclusions of the German P&T study (**P&T results based only on neutronics investigations**).

Toward phase-out scenario studies

Isotope	Ref.	GRS	IAEA
Pu vector (wt. %)			
Pu238	3.7	2.45	4.45
Pu239	46.4	52.49	57.17
Pu240	34.1	32.19	28.49
Pu241	3.8	0.9	0.6
Pu242	11.9	11.97	9.29
MAs vector (wt. %)			
Am241	75.5	63.8	62.09
Am242m	0.3	0.1	0.04
Am243	16.1	10.7	8.62
Np237	3.9	24.4	28.53
Cm243	0.1	0.0	0.03
Cm244	3.0	0.5	0.30
Cm245	1.1	0.5	0.33
Cm246	0.1	0.0	0.05



The **impact** on the trends of the **TRU vector** associated to the LWR SNF has been analyzed.

Some steps toward scenario optimization

NEW MIX

1st gen. :

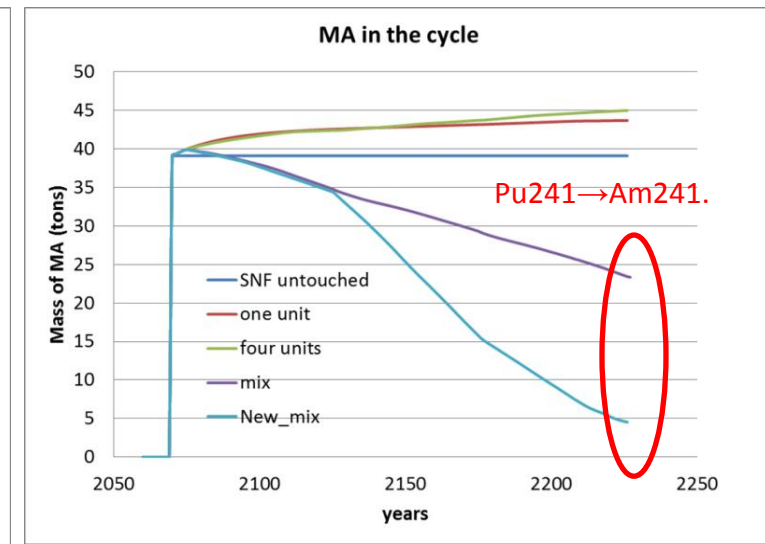
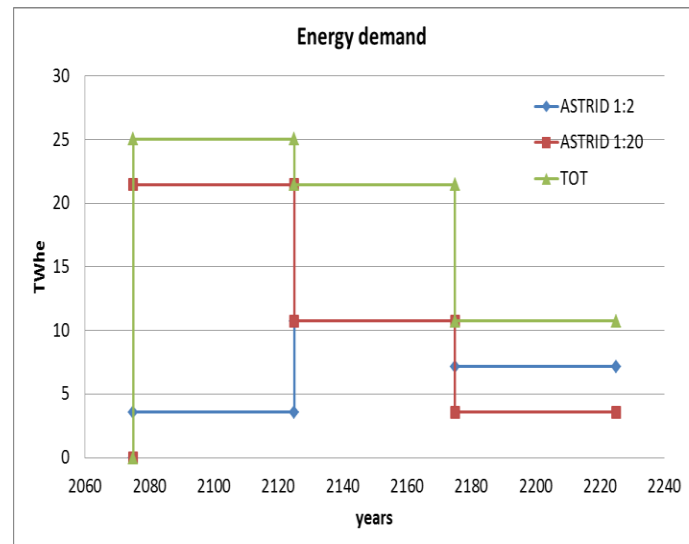
1 unit MA burner, 6 units Pu burner

2nd gen.:

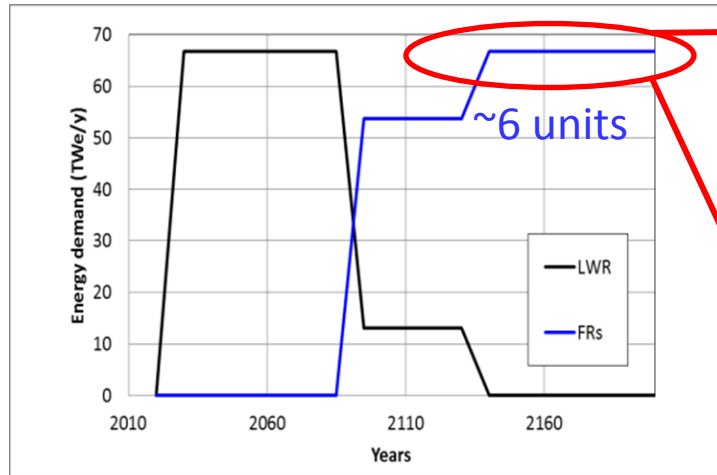
3 units MA burner, 3 units Pu burner

3rd gen.:

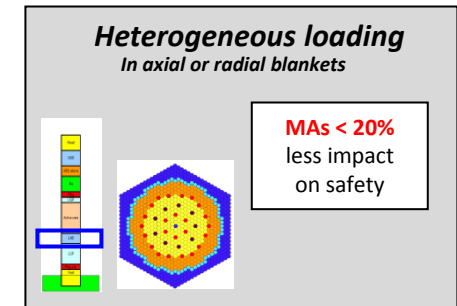
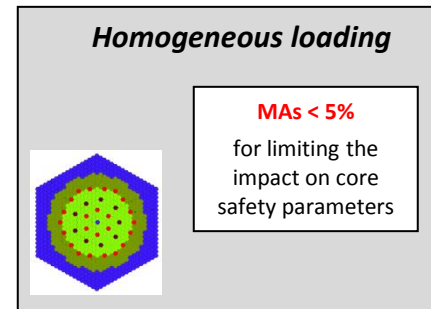
2 units MA burner, 1 unit Pu burner



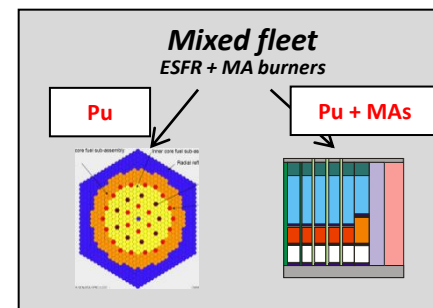
Simplified on-going scenarios (test case)



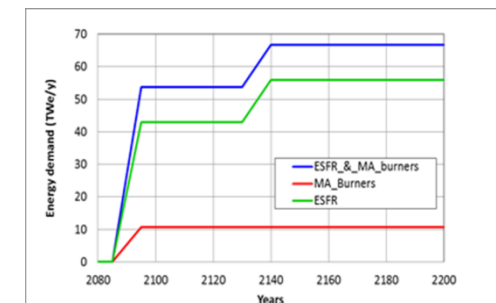
ESFR WH or ESFR CONF2



ESFR WH + ASTRID-like MA burner



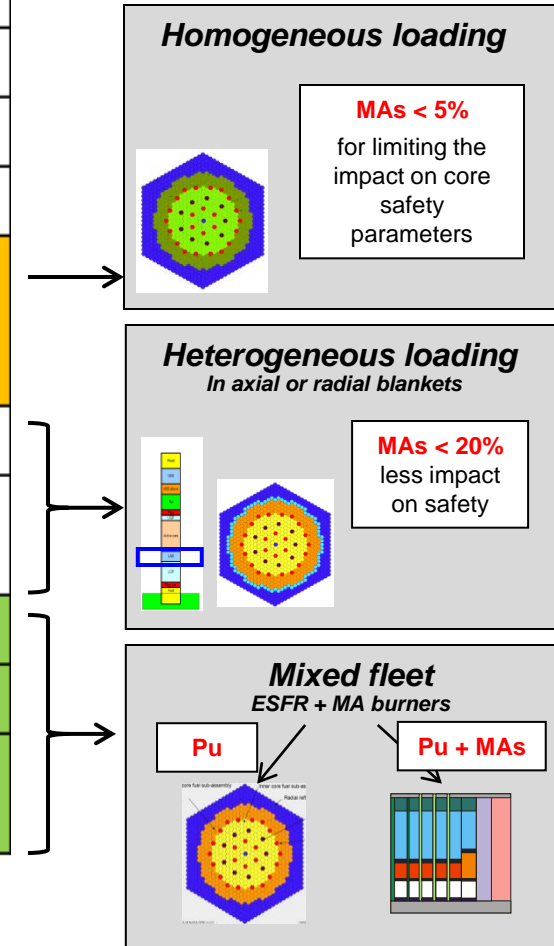
One ESFR unit → 3 MA burner units



Within the CP-ESFR project, the ESFR system (3600 MWth) was extensively studied by the IKET-TRANS group. Focus on safety - several measures for reducing the positive sodium void reactivity effect considered and a modified axial structure proposed – transient behavior confirm the better behavior of the optimized configuration with respect to the WH core.

Simplified on-going scenarios (test case)

Name	Type of System	Recycling			
		Pu	Am	Cm	Np
LWR	Thermal	No	no	no	no
ESFR (MOX)	Fast core – No Blankets	yes	no	no	no
ESFR (5 wt.% MAs in the core)	Fast core – No Blankets	yes	yes	yes	yes
ESFR-CONF2 (10 wt.% MAs in the blanket)	Fast core	yes	no	no	no
	Lower Axial Blanket (30 cm, 10 wt.% MAs)	no	yes	yes	yes
ESFR_ & MA burners	ESFR Fast core – No Blankets	yes	no	no	no
	MA Burner Fast core	yes	yes	yes	yes
	MA Burner Lower Axial Blankets (2 cm, 10 wt.% MAs)	no	yes	yes	yes

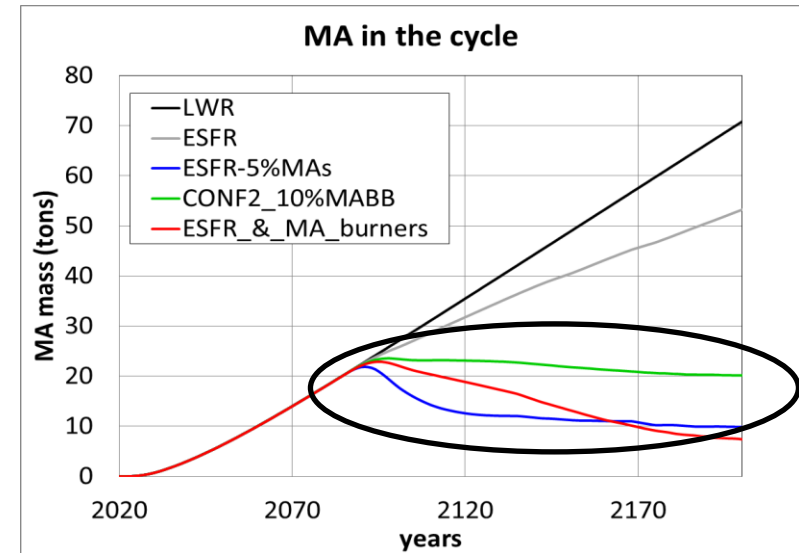
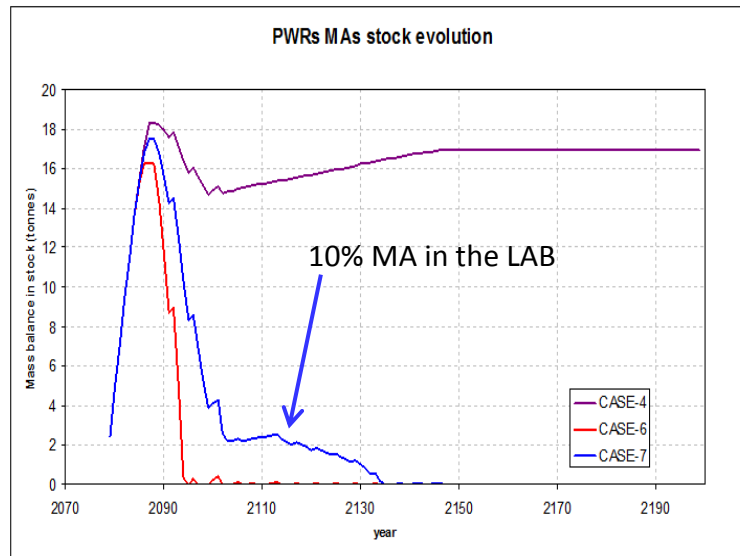


*B. Vezzoni, et al. „Innovative TRU burners and fuel cycles options for phase-out and regional scenarios”, Proc. Int. Conf. 13th IEMPT, Seoul, Rep. Korea, Sep. 2014.

Simplified on-going scenarios (test case)

Homogeneous
and
heterogeneous
MA loading
strategies have
been compared.

Focus remains
on safety*.



Mixed fleet → **more favorable from the safety point** of view due to a lower Na void reactivity effect in burner systems (-0.3\$) with MA-bearing fuels compared to larger ESFR-like ones (more than 4\$). Heterogeneous loading (10% MA) on CONF-2 allows stabilizing MA but Pu in the cycle accumulates.

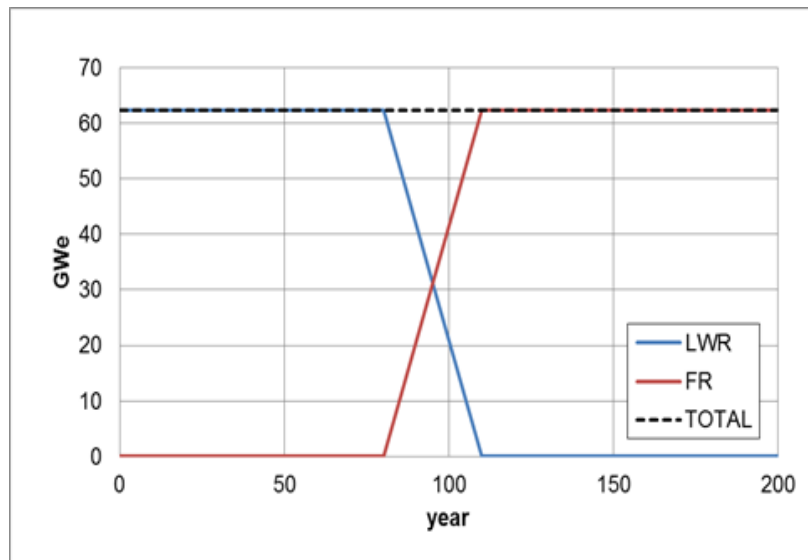
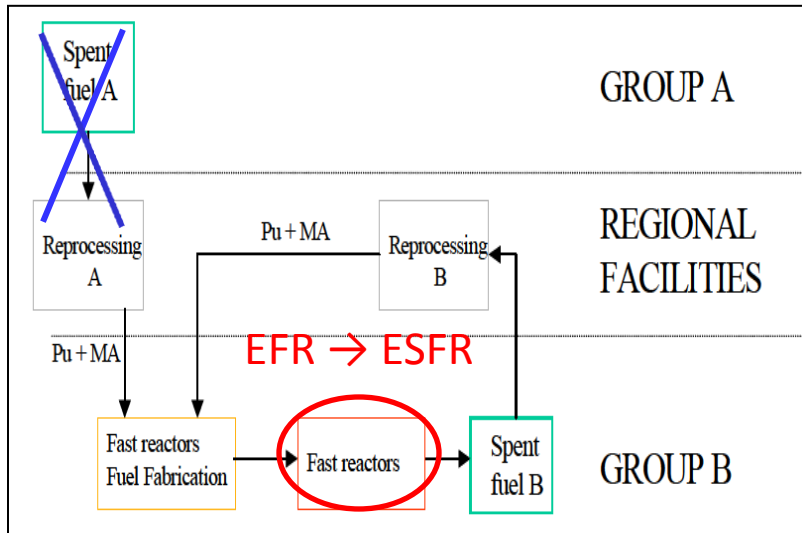
The **specific activity (TBq/t)** and the **specific decay power (W/t)** of the material in input to the fabrication plants remains **comparable with the case of a full fleet loaded homogeneously with 5% MAs in the core***/**.

*B. Vezzoni, et al. „Analysis of Minor Actinides incineration adopting an Innovative Fast reactor Concept”, Proc. Int. Conf. 12th IEMPT, Prague, Czech Rep., Sep. 2012.

**B. Vezzoni, et al. „Innovative TRU burners and fuel cycles options for phase-out and regional scenarios”, Proc. Int. Conf. 13th IEMPT, Seoul, Rep. Korea, Sep. 2014.

Activities on-going

Definition of the Regional Scenario



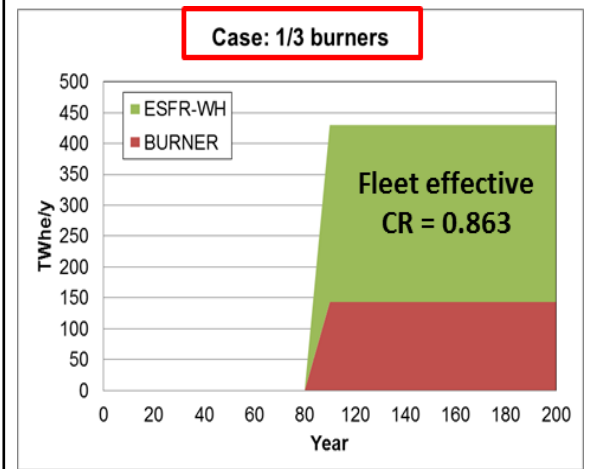
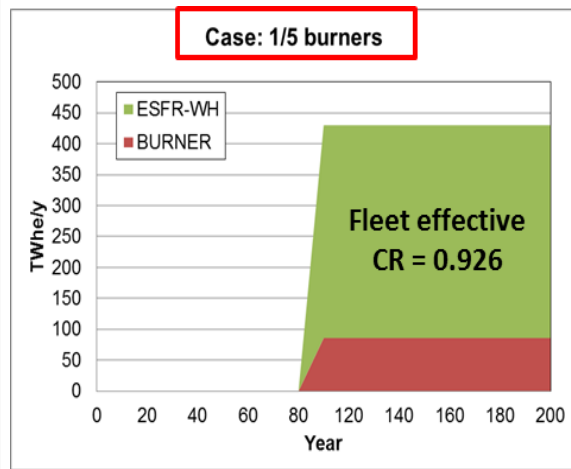
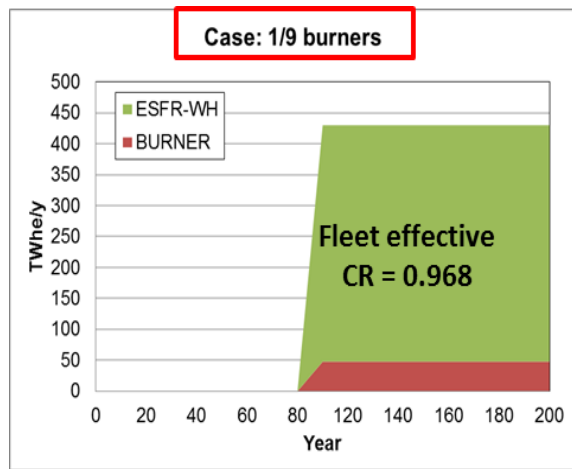
→ Modifications introduced with respect to PATEROS original scenario 3:

- The original **FR design** (EFR design) has been **substituted** by a more recent design: the **European Sodium Fast Reactor Design** developed within the FP7-CP-ESFR project,
- **No external SNF inventory** (simulating country in phase out) considered → neglected at first to focus mainly on reactor synergies → inserted in future studies.
- The overall **transition scenario** and **energy demand** considered in PATEROS has been **kept**.

ASTRID-like MA burners are introduced as **component of the FR fleet** (different shares see next slide)

Definition of the Regional Scenario

In combination with ESFRs



In combination with LWRs

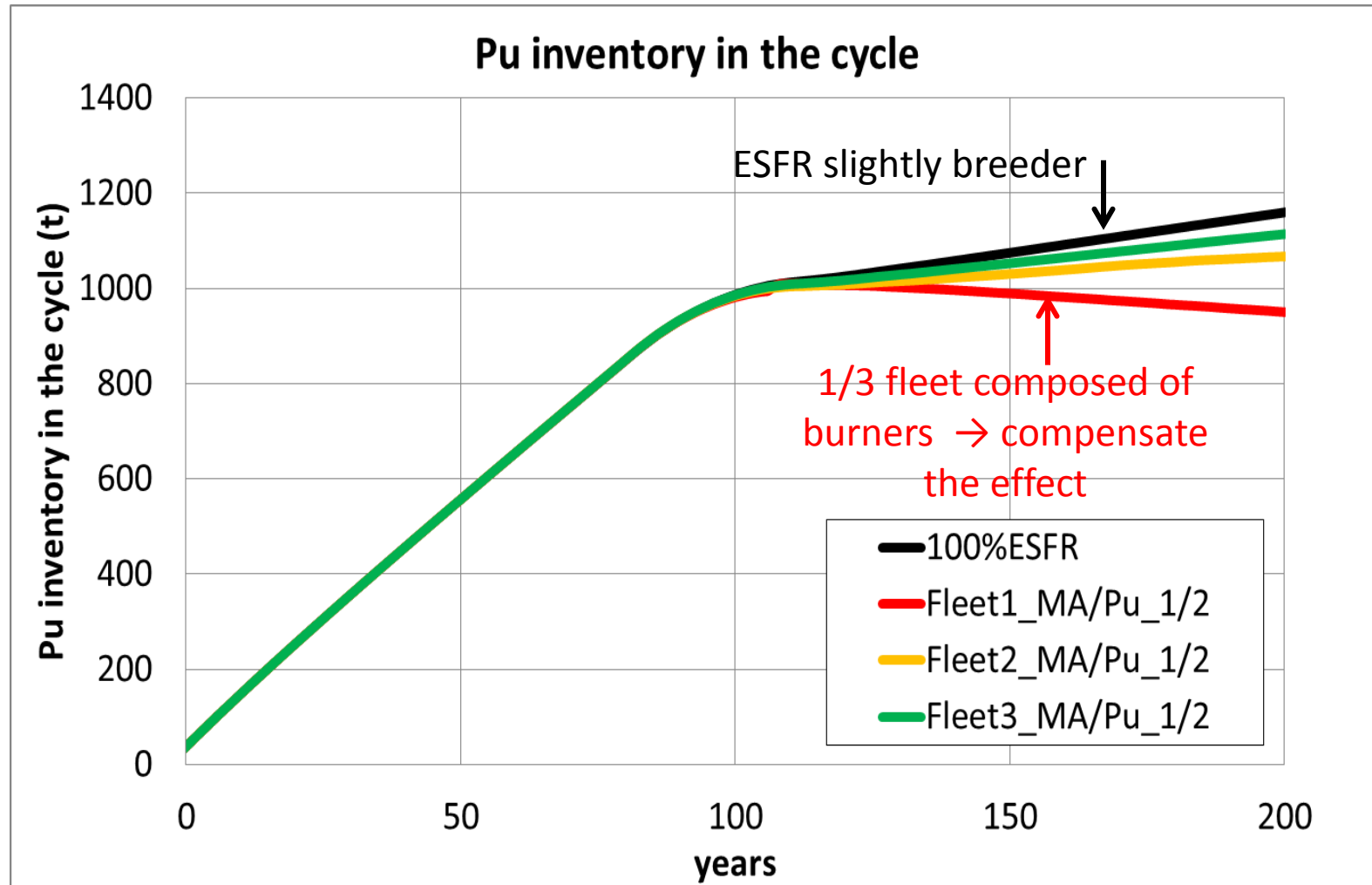
In order to try to take into account the effect induced by an external SNF inventory, we have considered setting aside ESFR systems but using only MA burners → different shares of LWRs remain in operation also during the second part of the scenario

1/9 fleet MA burners

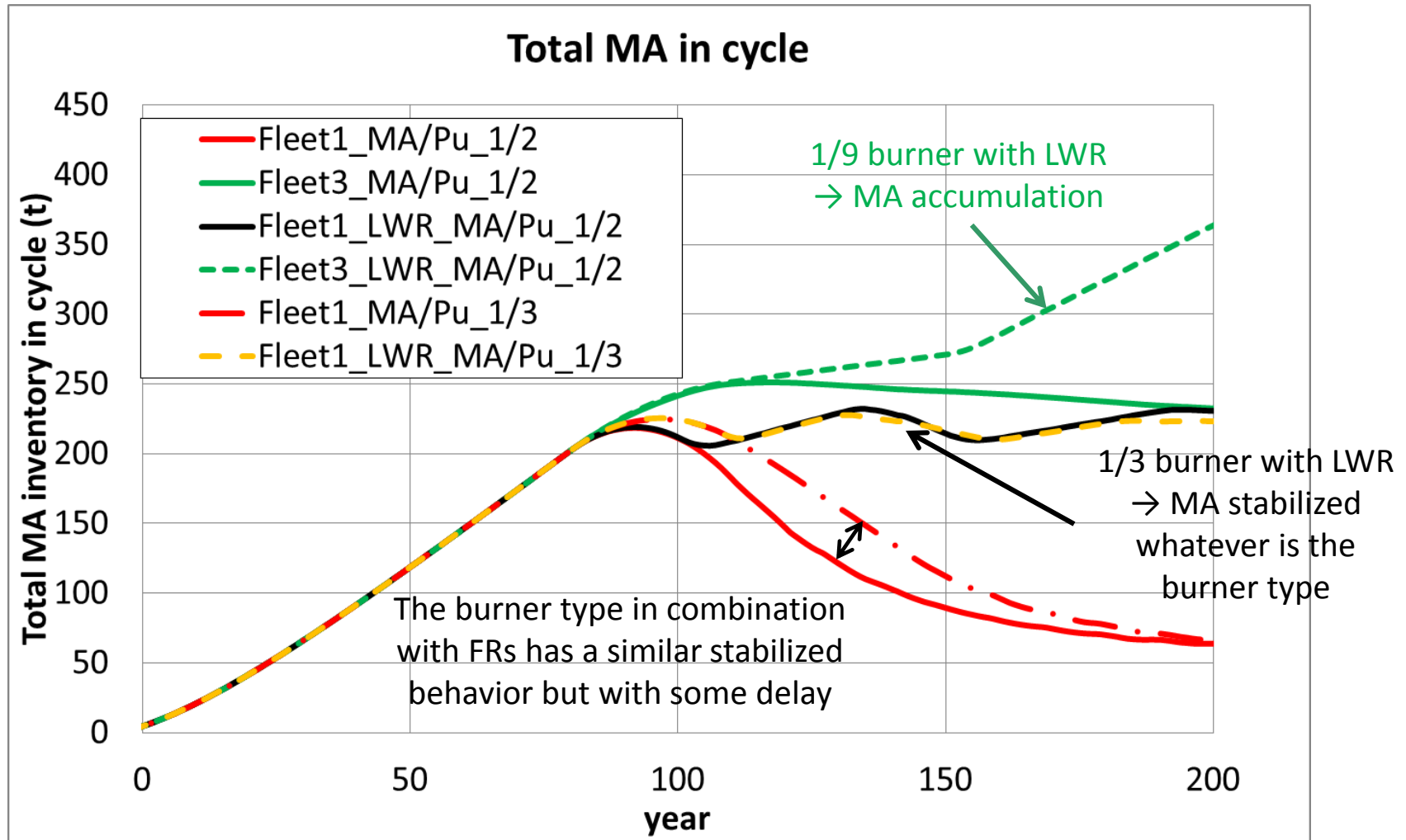
1/5 fleet MA burners

1/3 fleet MA burners

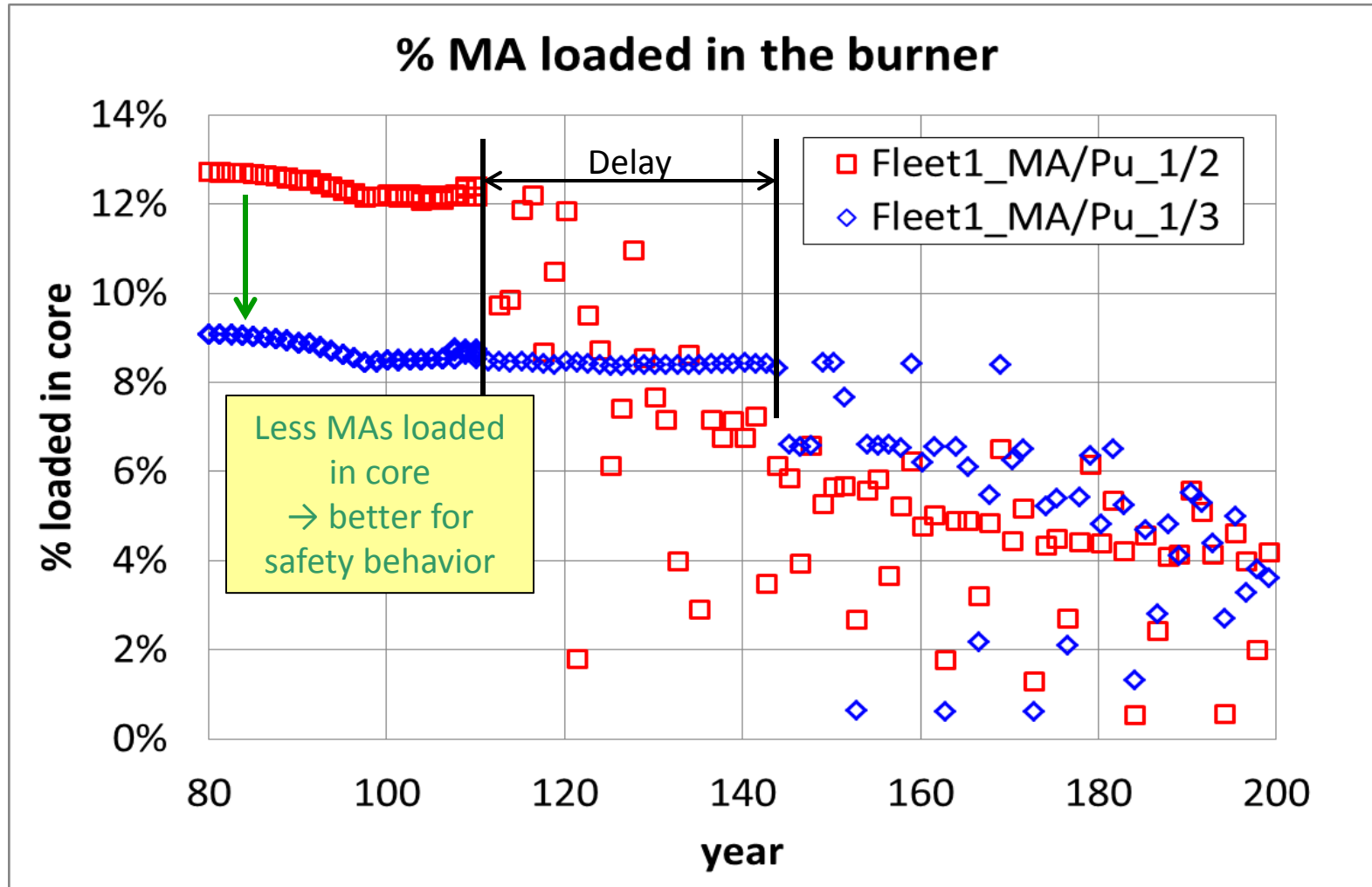
Regional Scenario: some results



Regional Scenario: some results



Regional Scenario: some results



Summary

Summary

The **IKET-TRANS** has been **continuously involved in several national/international activities on fuel cycle scenarios.**

Large experience has been acquired by the group. **The fuel cycle COSI6 code has been extensively adopted at KIT since 2007.** More than 10 different reactor types (LWR, ADS, SFR, LFR, Burners,..) have been considered in the studies. **For each system dedicated libraries (BBLs) have been generated at KIT** by means of ECCO/ERANOS codes for modeling the systems in COSI6.

Recently the group has been involved in the **German P&T study** by leading the scenario definition and comparison. The **activity on going is about ASTRID-like burner systems** to be implement in phase-out (regional) or on-going scenarios.

The activity on **fuel cycle and scenario calculations** for MA/TRU management has been **always complemented by safety investigation of the systems considered** in scenarios.

The **IKET-TRANS group** is contributing to present and future activities of the **OECD/NEA EG-AFCS.**

Thank you very much for your attention

The German P&T study (2012-2014)

- *Scenario 3 -4*: P&T implementation

	Reference system for German Scenario		Comparative technological option
	EFIT-like		ASTRID-like
Fuel	(IMF, TRUs)		(U,TRUs)
Matrix	MgO	Mo (natural)	UO ₂
Industrial experience	Limited	Limited	Wider
CR	0	0	(0.5 - 0.7)
Power (MWth)	400		~ 1200
Pu/MA ratio	~ 70/30 to -90/10		~ 70/30 to -90/10
Fuel Volume Fraction	~ 20 -30 %		100 %
Initial heavy metal loading (tons)	4-5 (TRUs)		18 (U +TRUs)
TRU Burning rates (kg/TWhth)	40-45		14-16
TRU burned / TRU loaded	~ 10%		~ 13%
Irradiation time (with 100% load factor ¹)	3 y		5 y
Number of units	7-8 units working for 150 y		7-8 units working for 150 y
Reprocessing (tons HM/y)	~ 9-10 (TRU)		~ 24 (U + TRU)
TRU cumulative losses	~ 1.7 tons		~ 1.7 tons
Variation of the amount of actinides and FPs in the storage	ca. 170 tons more		ca. 510 tons more
Energy (TWhth)	ca. 4000		ca. 12000

Definition of the Regional Scenario

The following cases have been considered:

CASE ID	Burner			FR/LWR
	type	share	GWe	
Fleet1_MA/Pu_1/2	MA:Pu=1:2	1/3	20.8	41.6 (ESFR)
Fleet1_MA/Pu_1/3	MA:Pu=1:3			
Fleet1_LWR_MA/Pu_1/2	MA:Pu=1:2			
Fleet1_LWR_MA/Pu_1/3	MA:Pu=1:3			41.6 (LWR)
Fleet2_MA/Pu_1/2	MA:Pu=1:2	1/5	12.5	49.9 (ESFR)
Fleet2_LWR_MA/Pu_1/2				49.9 (LWR)
Fleet3_MA/Pu_1/2	MA:Pu=1:2	1/9	6.9	55.5 (ESFR)
Fleet3_LWR_MA/Pu_1/2				55.5 (LWR)

The German P&T study (2012-2014)

Indicators	No P&T	No P&T but R&D	Regional implementation of P&T	P&T in Germany
Mass HLW (HM only)	212 t vitrified HLW 10500 t SNF at 2022	212 t vitrified HLW 10500 t SNF at 2022	212 t vitrified HLW 2 – 3 t of HM due to reprocessing losses	212 t vitrified HLW 3 – 4 t of HM due to reprocessing losses 3 t due to last transmuter
Thermal output after 50 y	$\sim 7.0 \times 10^6$ W	$\sim 7.0 \times 10^6$ W	$\sim 6.45 \times 10^6$ W	$\sim 6.45 \times 10^6$ W
Thermal output after 500 y	$\sim 2 \times 10^6$ W	$\sim 2 \times 10^6$ W	Reduced by 1-2 orders of magnitude	Reduced by 1-2 orders of magnitude
Radiotoxicity after 50 y	$\sim 1.4 \times 10^{12}$ Sv	$\sim 1.4 \times 10^{12}$ Sv	$\sim 1.4 \times 10^{12}$ Sv + relatively small contribution coming from 30-40 tons FPs due to transmutation	$\sim 1.4 \times 10^{12}$ Sv + relatively small contribution coming from 170 (ADS) or 525 (FR) tons FPs due to transmutation
Radiotoxicity after 500, 10000, 1000000 y	$\sim 5.0 \times 10^{11}$ Sv $\sim 7.0 \times 10^{10}$ Sv $\sim 9.0 \times 10^8$ Sv	$\sim 5.0 \times 10^{11}$ Sv $\sim 7.0 \times 10^{10}$ Sv $\sim 9.0 \times 10^8$ Sv	Reduced by 1-2 orders of magnitude	Reduced by 1-2 orders of magnitude

The German P&T study (2012-2014)

Indicators	No P&T	No P&T but R&D	Regional implementation of P&T	P&T in Germany
Secondary waste due to P&T	Not applicable	Not applicable	Short-lived intermediate level waste due to operation Long-lived waste due to reprocessing depends on the technologies used. An increase of the order of 5-10 times if compared to No P&T can be estimated Waste from decommissioning slightly increased Operational, reprocessing and decommissioning secondary waste can be shared in the regional scenario	Short-lived intermediate level waste due to operation Long-lived waste due to reprocessing depends on the technologies used. An increase of the order of 5-10 times if compared to No P&T can be estimated Waste from decommissioning slightly increased
Facility capacity/number requirements	Interim storage - geological repository for accommodating the above indicated quantities	Interim storage - geological repository for accommodating the above indicated quantities	Irradiation: 6-7 units for 30-40 years (e.g. 400MWth EFIT) Reprocessing and Fabrication: If TRU elimination in ~30-40 y 15 t HM/y for EFIT-like if time span longer (~150 y) Geological repository in Germany for accommodating FP and losses	Irradiation: 7-8 units for 150 years (400MWth EFIT-like or 1200 MWth ASTRID-like) Reprocessing and Fabrication: 9-10 t HM/y for EFIT-like or 24 t HM/y for ASTRID like Geological repository in Germany for accommodating FP and losses
Facility requirements to comply with accepted dose limits	Associated to interim storage	Associated to interim storage	At reprocessing, fabrication and irradiation plants ad hoc technological solution to limit the dose to workers can be considered as part of P&T additional costs	At reprocessing, fabrication and irradiation plants ad hoc technological solution to limit the dose to workers can be considered as part of P&T additional costs

The German P&T study (2012-2014)

Indicators	No P&T	No P&T but R&D	Regional implementation of P&T	P&T in Germany
R&D requirements	Interim storage - geological repository	Interim storage - geological repository + specific R&D activities in international context to understand issues on P&T	Interim storage - geological repository + R&D on P&T: e.g. design of transmutation device and fuel, materials, thermal-hydraulics, safety, decommissioning reprocessing	Interim storage - geological repository + R&D on P&T: e.g. design of transmutation device and fuel, materials, thermal-hydraulics, safety, decommissioning reprocessing
Uranium inventory	9710 t	9710 t	9710 t or less if recovered U is used by on-going countries	9710 t
Knowledge availability	R&D Knowledge in all relevant technical area is presently available but it could be progressively lost	R&D knowledge in selected technical area should be developed	R&D knowledge in all relevant technical areas Design, construction, operational and decommissioning knowledge can be shared at EU level	R&D knowledge in all relevant technical areas as well as further design, construction, operational and decommissioning knowledge will be needed